

# **MICROPROCESSOR BASED RAIL-AXLE COUNTING AND HOTBOX DETECTION SYSTEM**

**A Thesis Submitted  
In Partial Fulfilment of the Requirements  
for the Degree of  
MASTER OF TECHNOLOGY**

**by  
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**to the  
DEPARTMENT OF ELECTRICAL ENGINEERING  
INDIAN INSTITUTE OF TECHNOLOGY, KANPUR  
JULY, 1982**

dedicated to

my parents

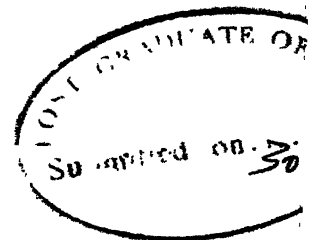
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### CERTIFICATE

Certified that the work entitled 'MICROPROCESSOR BASED RAIL AXLE-COUNTING AND HOTBOX DETECTION' by Dama Venkata Rama P has been carried out under my supervision and has not been submitted elsewhere for the award of a degree.

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## ABSTRACT

Hotbox detection and signalling are two important aspects that Railways are very much concerned about. Improved techniques for this purpose are called for because of the need to increase the traffic and speed. Microprocessor based Rail axle counting and hotbox detection system is one such system incorporating advanced techniques with built in safety against human error. The thesis contains the software for a Motorola 6800 microprocessor based system around which the axle counting and hotbox detection system is proposed. The software is developed and tested successfully by simulating real time signals using a toytrain.

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## CHAPTER 1

### INTRODUCTION

Railways, being an essential part of infrastructure constitute the nerve centre of our economy bearing a lot of strain. What with increasing prices and fast depleting sources of crude oil coupled with abundant national reserves of coal and seemingly exponential growth in population, it is imperative that the strain should multiply. But it has to be borne; borne with increased efficiency and perfect safety. However, it is disturbing that of late railway accidents have become common place and most often these are traced to signal failures. Lest the economic growth and human life would be in peril, improvement in signalling schemes should be immediately attended to. In this age of computers and 'quick thinking' what else other than micro-processors can comfortably step in! All along this has been the motivating factor.

Since the very beginning of railways the basic aim of signalling is, to monitor a prescribed length of track and give an indication about the occupancy of that particular length of track. Another important direction in which railways were and still are concerned is hotbox detection - which occurs when inadequate bearing lubrication or mechanical flaws

cause a significant increase in wheel temperature. As the bearing temperature rises to an abnormally high level, a bearing failure results. Such bearing failures constitute a major cause of car derailment, endangering life, destroying property, resulting in costly delays and maintenance. Continuous studies and changes in implementation are going on regarding these.

Increasing traffic and higher speeds call for improved control and safety. Current trends in the field of micro-computers, especially the development of very cheap, powerful and reliable microprocessors with elaborate support systems, has made the introduction of computer technology into railway signalling and control inevitable.

This thesis titled 'MICROPROCESSOR BASED RAIL AXLE COUNTING AND HOTBOX DETECTION SYSTEM' mainly aims at software development of combined system for signalling through axle counting and hotbox detection system. The software is developed and tested successfully by simulating real time signals using a toy train. The software<sup>15</sup> developed for Motorola 6800 microprocessor based system.

## 1.1 OVERVIEW OF THESIS :

### CHAPTER 2 :

In this chapter various conventional methods of signalling and hot box detection systems are described. Their merits and demerits are discussed.

### CHAPTER 3 :

In this chapter a new scheme that implements signalling through axle counting and its advantages over the conventional signalling schemes are discussed.

### CHAPTER 4 :

This chapter describes the details of infrared hotbox detection system.

### CHAPTER 5 :

This chapter gives the specifications of the system, how they are proposed to be met and the approach taken in the development of the software. This chapter also gives a proposed layout of the transducers at the track side.

### CHAPTER 6 :

This chapter gives detailed description of the developed software.

### CHAPTER 7 :

The thesis is concluded with a critical review of the present work and suggestions for future work.

## CHAPTER 2

### CONVENTIONAL SIGNALLING SCHEMES AND HOTBOX DETECTION SYSTEMS

In this chapter, various conventional signalling schemes, their principles of operation, merits and demerits are discussed. First various signalling methods are discussed later hotbox detection system is discussed.

#### 2.1 CONVENTIONAL SIGNALLING SCHEMES

##### 2.1.1 Track Circuit - Noncoded DC

The track circuit is the most important link in most signalling systems. It is the vital connection between the train and the rest of the signal system. The track circuit enables us to know just where a train is in a given section of the track. But most important of all the track circuit enables us to provide maximum protection for train movements. ugh the track circuit we can indicate the following :

1. The block is occupied
2. There is no broken rail
3. It is safe to proceed at authorized speed

Track is made of sections and each section is insulated the other section by wax-coated hard vulcanised fibre. In [3] Fig. 2.1.1a track circuit is shown with a neutral track relay,

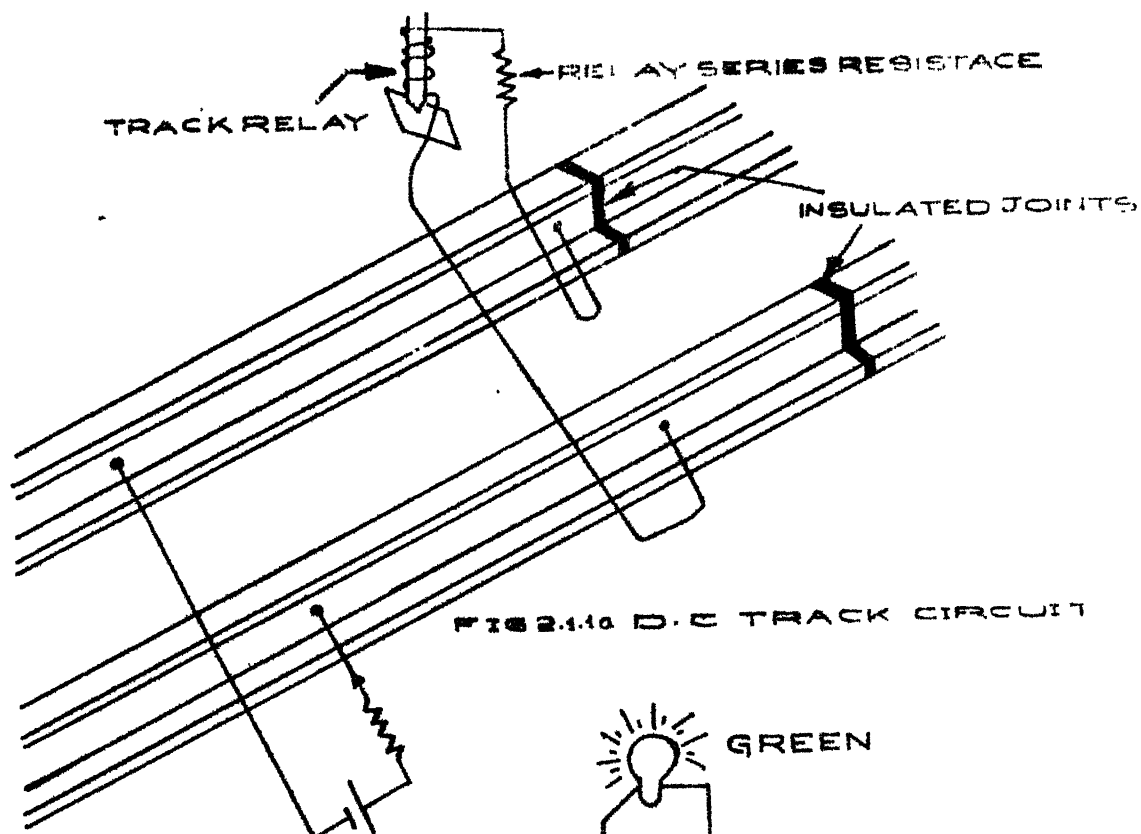


FIG 2.1.1a D.C TRACK CIRCUIT

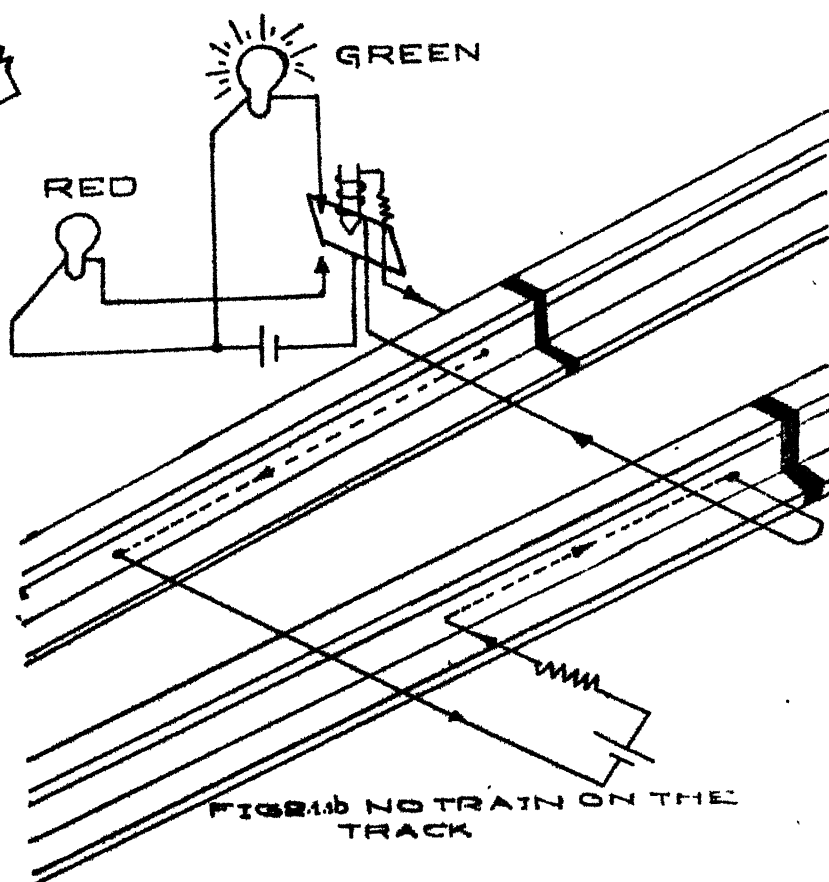


FIG 2.1.1b NO TRAIN ON THE TRACK

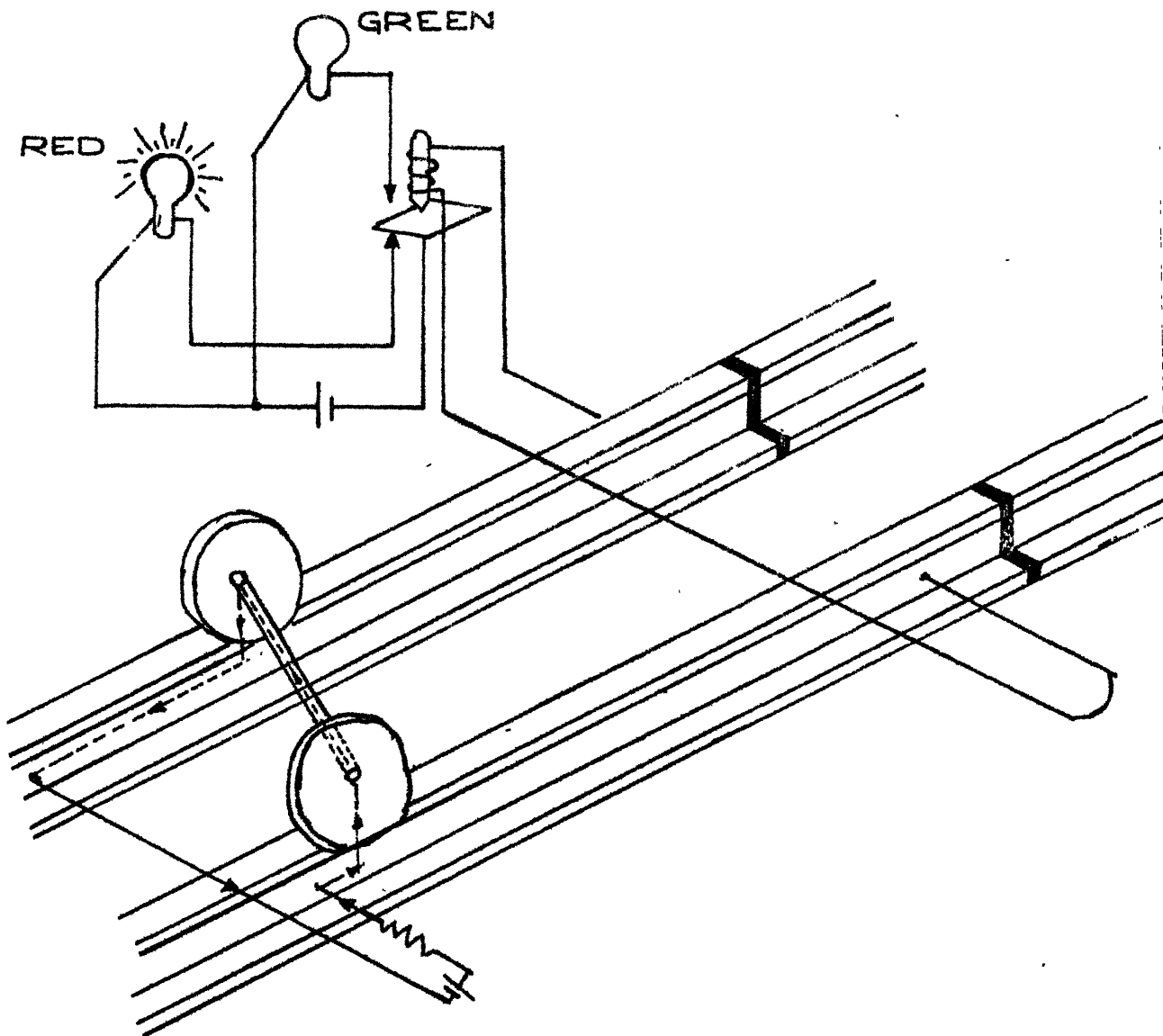


FIG. 2.1.1c TRACK IS OCCUPIED (DC TRACK CKT)

which will be energised when sufficient current flows through its coils, regardless of the direction of current flow or polarity of the circuit.

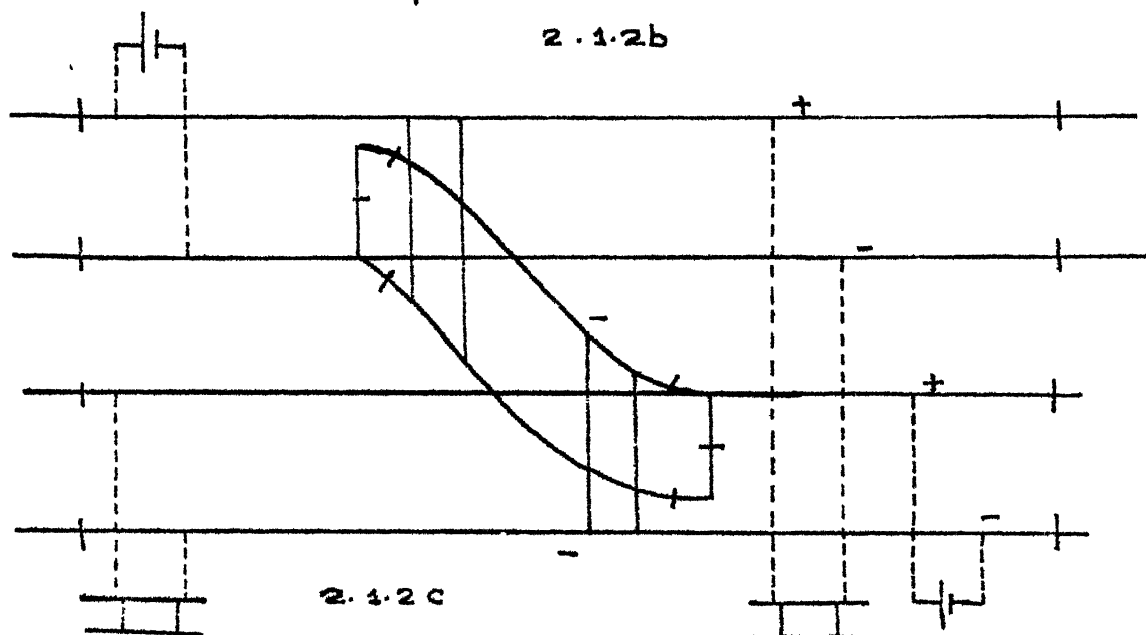
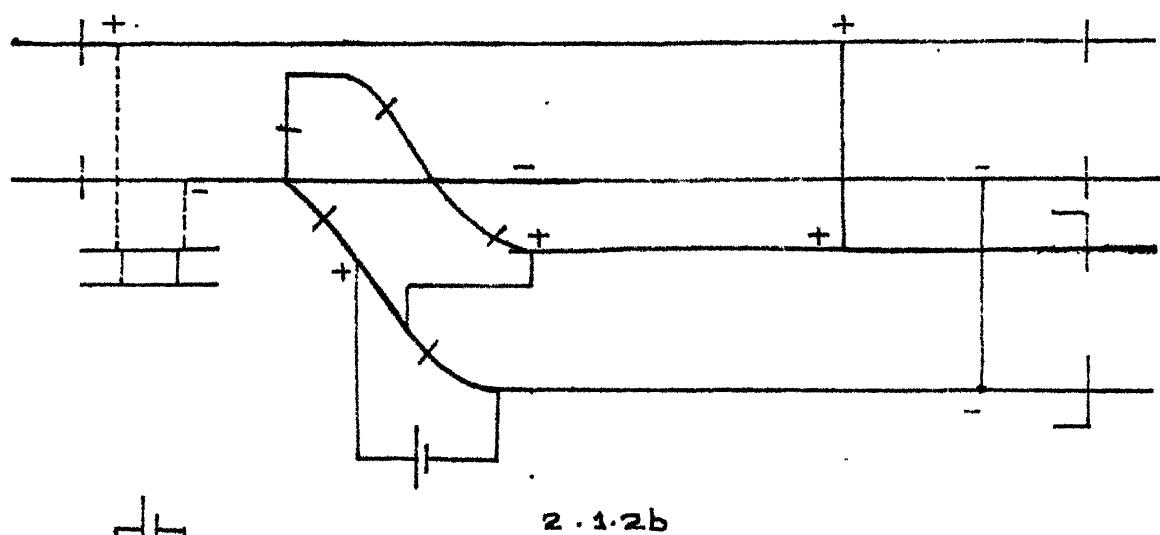
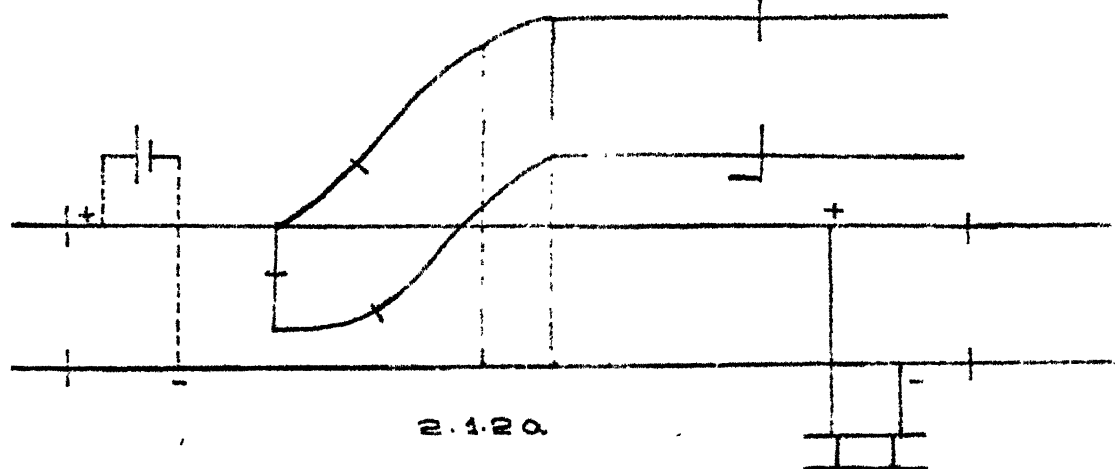
The track circuit operation can be understood from [4] Figs. 2.1.1b and 2.1.1c. Figure 2.1.1b shows the direction of current flow when there is no train on the track section, which energizes the relay, green light is glown, indicating that the track section is CLEAR. When train enters into the track section (Fig. 2.1.1c) it shunts the track relay. With this effect relay is released allowing red light to glow, indicating occupancy of the track section.

#### 2.1.1.1 Crossover (Fouling) Connections Using Noncoded DC Track Circuit

Since the track circuit is used to detect trains within its limits, it must also detect the presence of trains or cars that are too close to permit safe passage. This is done by extending the track circuit limits to the points of fouling along the track circuit.

Figure 2.1.2a illustrates one type of fouling circuit used. That portion of the turnout, within which a car will foul the main line, is connected to track circuit in multiple. The presence of a car on this fouling section will shunt the track relay. When this type of circuit is used, it is essential that the fouling connectors are maintained in good

## FIG 2.1.2 FLOODING CIRCUITS





condition. Breakage of these connectors will result in loss of shunt protection on the fouling section of turn out.

Figure 2.1.2b illustrates another type of fouling circuit used. The fouling section of the turn out is connected in series with the track circuit. This circuit has the advantage of better protection in case of any breakage of fouling connector or a rail as the track circuit will be opened and the track relay will be de-energised.

Figure 2.1.2c illustrates a method used to provide fouling protection on crossovers. The fouling connectors are located so as to connect the fouling sections in multiple with the main track similar to a turn out. The fouling protection on the upper track extends to the insulated joints in the center, as does the fouling protection on the lower track.

#### 2.1.1.2 Considerations to be taken for Installations of DC Track Circuits

'Ballast leakage' is an ever-present factor, which causes a reduction in flow of current to the track relay. It refers to that part of the track current that flows or [5] leaks from one rail to another through the ties, ballast and ground. It is desirable that the ballast resistance to be maintained as high as possible. Fig. 2.1.3a gives simplified drawing of track circuit, the battery, the limiting resistance, the rails, the insulated joints and the relay. Actually the

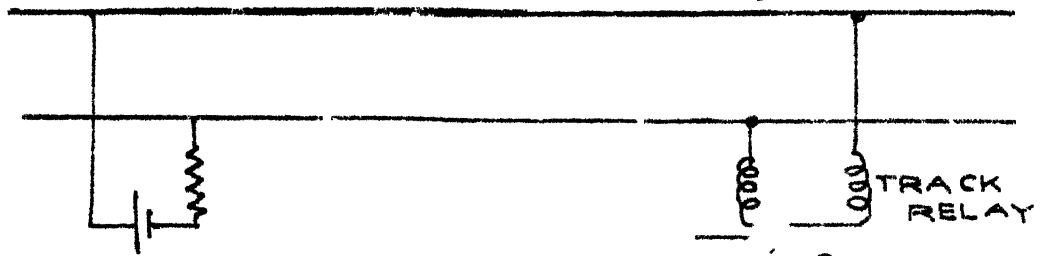


FIG. 2.1.3a D C. TRACK CIRCUIT

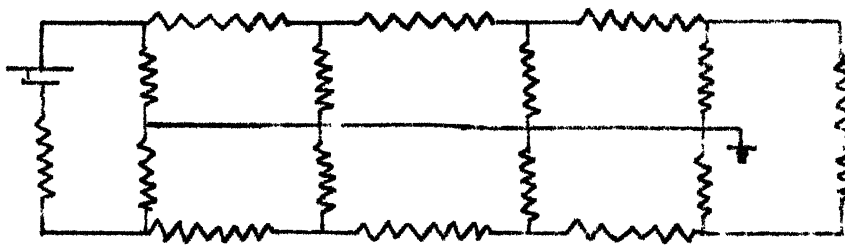
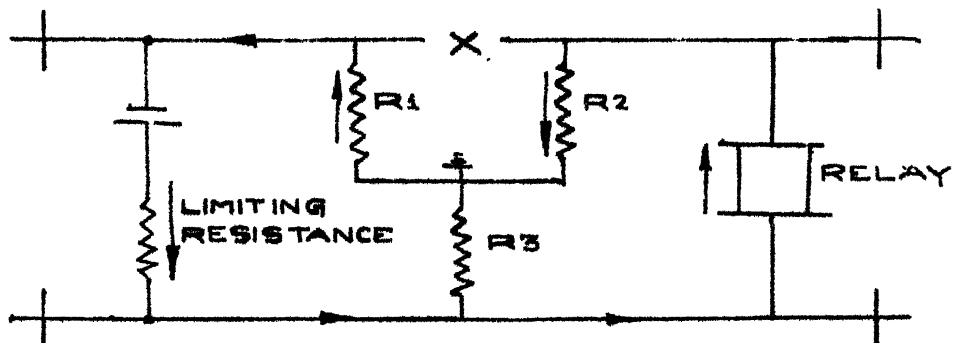


FIG. 2.1.3b BALLAST RESISTANCES

FIG. 2.1.3c BALLAST RESISTANCES  
(BROKEN - RAIL)

circuit is a network of resistances as shown in Fig. 2.1.3b, the limiting resistor at the battery, the resistance of the rails, the resistance of the relay and the resistance between the rails which is sum of the resistances of each rail to ground.

All this must be taken into consideration when adjusting a track circuit. Bonded rail resistance ordinarily varies from 15 thousandth to 4 hundredths (0.015 to 0.04) ohms per 1,000 ft of track. Ballast resistance may vary from less than one to hundreds of ohms per 1,000 ft of track. In wet weather, ballast resistance usually lessens. In dry or freezing weather it increases.

A ballast resistance network with a rail broken is shown in Fig. 2.1.3c.  $R_1$  is the leakage resistance from the battery side of the broken rail to the ground.  $R_2$  is the leakage resistance from the relay side of the broken rail to the ground.  $R_3$  is the leakage resistance from the opposite rail to the ground.

It will be seen that there are two paths for current from the battery. One is through the limiting resistance and leakage resistances  $R_3$  and  $R_1$ . The other is through the limiting resistance, the relay and leakage resistances  $R_2$  and  $R_1$ . As ballast resistance varies, there may be a relatively critical range of ballast resistance where sufficient current

may flow through the path including the relay to cause improper operation of the relay if the circuit is not properly proportioned or adjusted.

The following are the disadvantages of DC track circuits.

1. When a train longer than the track circuit comes on the track, track circuit will give release when the forward wheels clear the track circuit, and before the rear wheels enter the circuit. The obvious solution is the lengthening of the track circuits themselves but this merely exchanges the problems rather than solving them. Firstly, the cost of lengthening all of the track circuits in a hump yard is prohibitive and in addition, it will defeat our attempts to handle a greater volume of traffic. Thus, the requirements for higher traffic handling are best met by short track circuits while the requirements for handling long cars are the exact opposite.
2. The presence of oil and grease is making the track circuit with light boxer cars distinctly marginal.

#### 2.1.2 Loop Track Circuits

The disadvantages connected with DC track circuit as mentioned above led the loop track circuits to be in use. The design requirements of the loop track circuits are as follows :

1. It should see a car immediately as it enters the area of the loop surrounding the switch, irrespective of the direction or speed of travel.

2. It should continue to see this car until it had cleared the loop completely.
3. If the car stops over the loop it should continue to see it for an indefinite period.
4. Its method of operation must be fail safe in that a failure of any of the components would automatically drop the relay to a locked position .
5. It must not be sensitive to the normal changes of climate to which it will be subjected in a yard, i.e., variations of temperature and humidity and the presence of snow, water or ice.
6. It should have no moving parts, maintenance should be an absolute minimum and the adjustment should require no special skills beyond those normally possessed by a signal technician and with equipment which he would normally be expected to possess.

#### 2.1.2.1 Operation

Briefly, the unit contains two oscillators (Fig. 2.1.4a), one called the loop oscillator and the other the reference oscillator. The loop oscillator is tuned to approximately 94 KHz while the reference oscillator is tuned to approximately 89 KHz. The output of these two oscillators is fed into a mixer which has as its inputs the two oscillator frequencies and gives as its output a frequency which is the difference between

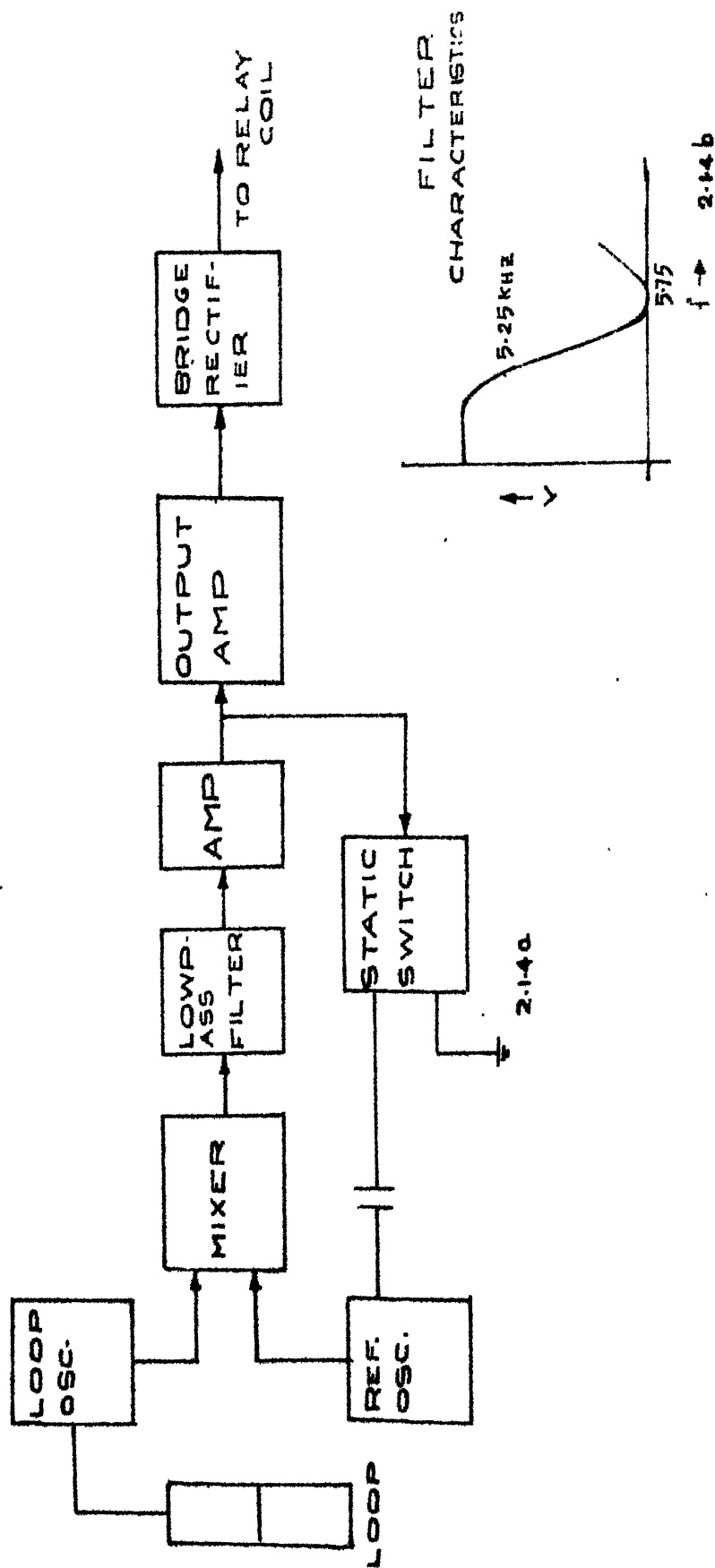


FIG. 2.1.4 LOOP TRACK CIRCUIT

them, in this case approximately 5 KHz. This 5 KHz signal is fed through a lowpass filter which has a cut off at approximately 5.25 KHz to a two stage amplifier followed by a push pull output stage. This output signal, still at 5 KHz is rectified in a bridge type rectifier and the DC voltage so developed is utilized to energize the operating relay.

When a car goes over the loop its inductance is reduced and because this loop is part of the tuned circuit of the loop oscillator, frequency rises by an amount which depends on the dimensions of the vehicle but will be of the order of 500 to 2000 Hz for typical box cars. The reference oscillator remains at its original frequency with the result that the difference frequency as seen by the mixer rises from 5 KHz to some higher value, for example, 6 KHz. When the frequency of this difference signal is applied to the lowpass filter, it is no longer passed by this filter, which cutsoff at 5.25 KHz and the output is thereby removed from the relay.

When the boxer leaves the loop, the loop oscillator returns to its original frequency, the difference frequency drops below 5.25 KHz and the filter then once again passes it and the relay is picked up.

The cutoff slope of the lowpass of filter is made as steep as possible so that the action is suitably rapid but it was felt desirable to introduce what might be described as a toggle action to ensure a positive snap to the switching action.

To achieve this, a portion at the output of the amplifier is rectified and the DC voltage is used to hold open a transistor static switch. This switch puts across the reference oscillator an additional capacity when the voltages falls as the increase in frequency pushes over the edge of the slope. The effect of the increasing capacity on the reference oscillator is to lower the frequency of this oscillator at the same movement we are raising the frequency of the loop oscillator and the difference frequency is thereby violently increased and a sharp switching action takes place as soon as the signal through the filter has dropped by 3 dB.

The DC voltage holding up the operating relay is derived from the 5 KHz signal. This signal is made by utilizing the two oscillators and taking the difference frequency between them. Should either oscillator fail, then the difference frequency would become 90 KHz well beyond the filter cutoff and therefore the relay must drop into the safe position. Should any of the amplifying chain along the way develop a defect, this can only result in a reduction of the amplifier gain and this again would remove the voltage to the relay thereby dropping it to a safe position.

A failure of the power supply would also, of course, drop the relay and as a matter of fact, it can be kept in a place, provided the entire chain of operation is in order. A



A failure of the loop caused by mechanical damage would, of course, disconnect the inductance of the loop oscillator.

The following are the disadvantage of this scheme :

1. Existence of insulated joints, which needs continuous supervision and maintenance of these joints.

### 2.1.3 Shunt Overlay Track Circuit

Shunt overlay track circuit operates without interference from other track signals and does not require insulated joints and is also failsafe.

In its simplest form, the shunt overlay track circuit consists of a section of track with transmitter connected to one end of the track section and a receiver and relay [2] connected at the other end (Fig. 2.1.5a). It functions very much like the DC track circuit except that the battery is replaced by a transmitter. The receiver consists of an amplifier rectifier and filter in addition to the track relay. Like the DC track circuit, the track relay remains energised as long as the receiver finds a signal (above a certain level) on the track. The presence of a train in the track section will be detected by virtue of the electrical shunt the train produces across the track.

As in the DC track circuit, the operation of the shunt overlay track circuit is hampered by ballast resistance and

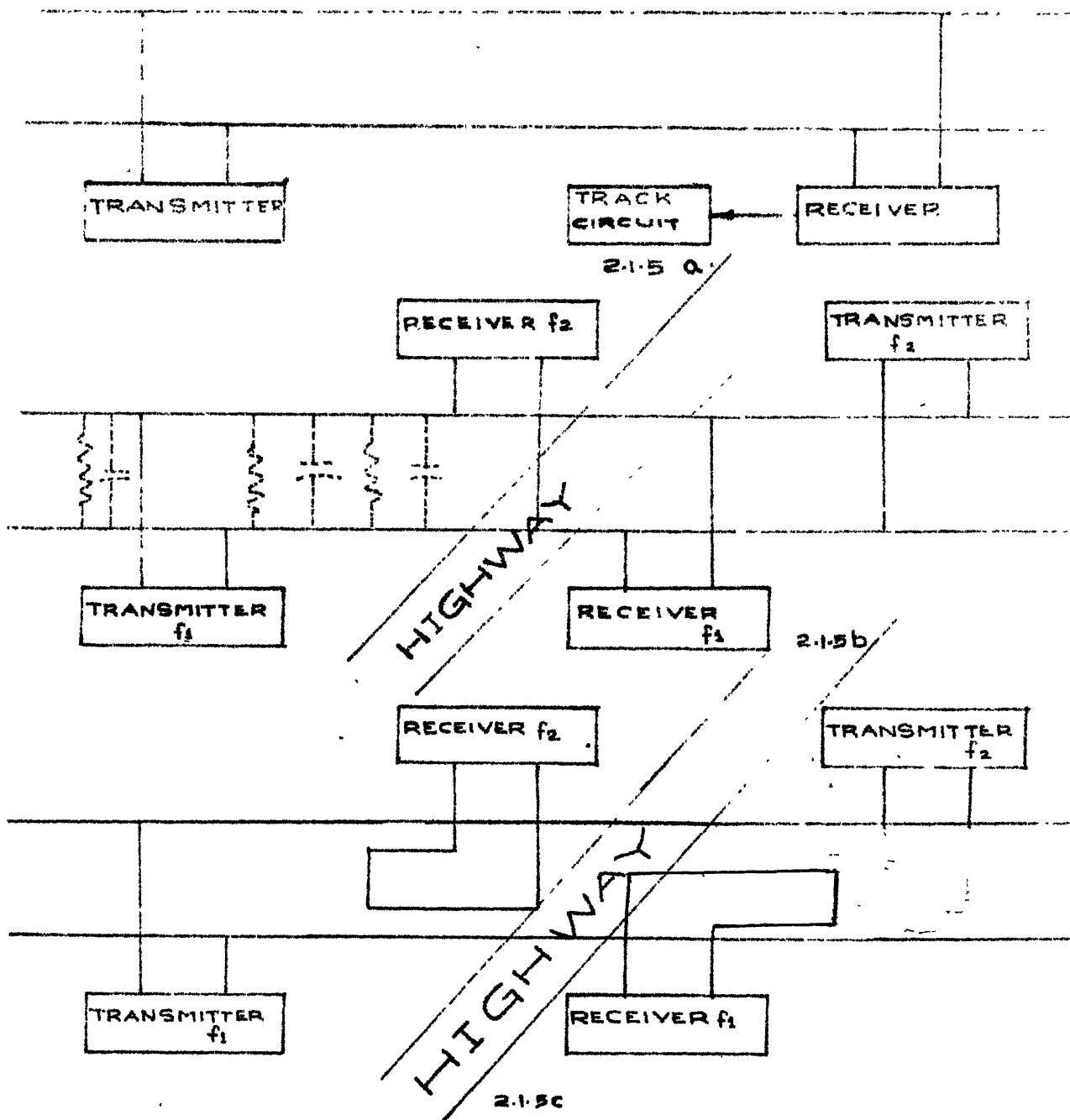


FIG 2-1-5 HIGHWAY CROSSING

the changes in that resistance. For proper operation, the receiver must be capable of 'hearing' the transmitter in the absence of a train and with the ballast resistance low. Yet the receiver must not be able to 'hear' the transmitter in the presence of a train and with the ballast resistance high. Inter-rail capacitance effects are relatively negligible upto a transmitter frequency of about 5 KHz. Most ballasts will run (at its lowest) 5 ohms per 1,000 ft or better. Shunting resistance of a train is generally accepted to be less than 0.06 ohms. Under these conditions, a shunt overlay circuit can be made to operate over 4,000 ft. without difficulty. It is possible to make longer track circuits under somewhat ideal conditions, say upto 10,000 ft. but safe operation is no longer assumed.

In Fig.2.1.5b is shown a single section of track arranged for double direction running with a highway crossing and two overlay track circuits arranged so that they overlap at the crossing. A train shunting the track between transmitter f1 and receiver f2 will indicate track occupancy in receiver f1 but not in receiver f2 : a train shunting the track between receiver f2 and receiver f1 will indicate track occupancy in both receivers; and a train shunting the track between receiver f1 and transmitter f2 will indicate track occupancy in receiver f2 but not in receiver f1.

When a train approaching the crossing from the direction of transmitter f1 it will activate the crossing flashers as soon as track circuit is occupied between transmitter f1 and receiver f1. This same circuitry will keep the flashers operating until the train passes over the crossing and clears receiver f1. Fig.2.1.5b shows symbolically the ballast resistance and internal capacity.

One of the objections to overlay track circuits that is frequently raised is that they do not have a sharply defined 'clear-out' as compared to DC track circuits. After train has passed the receiver and is receding, it still provides a fairly good shunt of the interrail voltage even though the receiver is between the transmitter and the train. How effective a shunt the train provides depends upon ballast resistance. For this reason the 'clear-out' point will vary from about 2 to 75 ft beyond the point of connection of the receiver, depending upon ballast resistance.

If greater resolution than this is required, the receiver may be coupled to the track by virtue of a loop as shown in Fig.2.1.5c. These loops are each 50 ft in length and approximately the width of the track gauge. The loops couple the rail current to the receiver. In the absence of a train, rail current is coupled to the receiver and keeps the track relay energized. When a train enters the track circuit, it

shunts the rail current and track relay indicates 'occupancy'. Now, however, after the train passes the loop and is receding, it provides an excellent shunt beyond the receiver loop, causing a heavy flow of rail current and the receiver re-operates its associated track relay. The 'clear-out' point of loop-coupled receiver will vary with ballast resistance from the centre of loop to the end, that is from 0 to 25 ft.

The following are the drawbacks :

1. Loop is costlier to install and maintain.
2. When ballast resistance is unusually high, insufficient rail current will flow, thus the receiver gets insufficient signal to keep the track relay operated. This can be corrected by placing tuned shunts across the track as shown symbolically by dotted lines in Fig. 2.1.5b. These are fail safe since their loss will cause an 'occupancy' indication.
3. From the discussion of Fig. 2.1.5 it becomes obvious that transmitter/receiver pairs must be selective so that the receiver responds only to its own transmitter. Disadvantage is that the interference signals are additive. That is, interference signals which can produce distortion products (that lie within the pass-band of the filter) will result in a filter output which adds to the relay current. Naturally, if there are enough of these distortion products, they will produce unsafe condition by providing track relay current in the absence of a legitimate

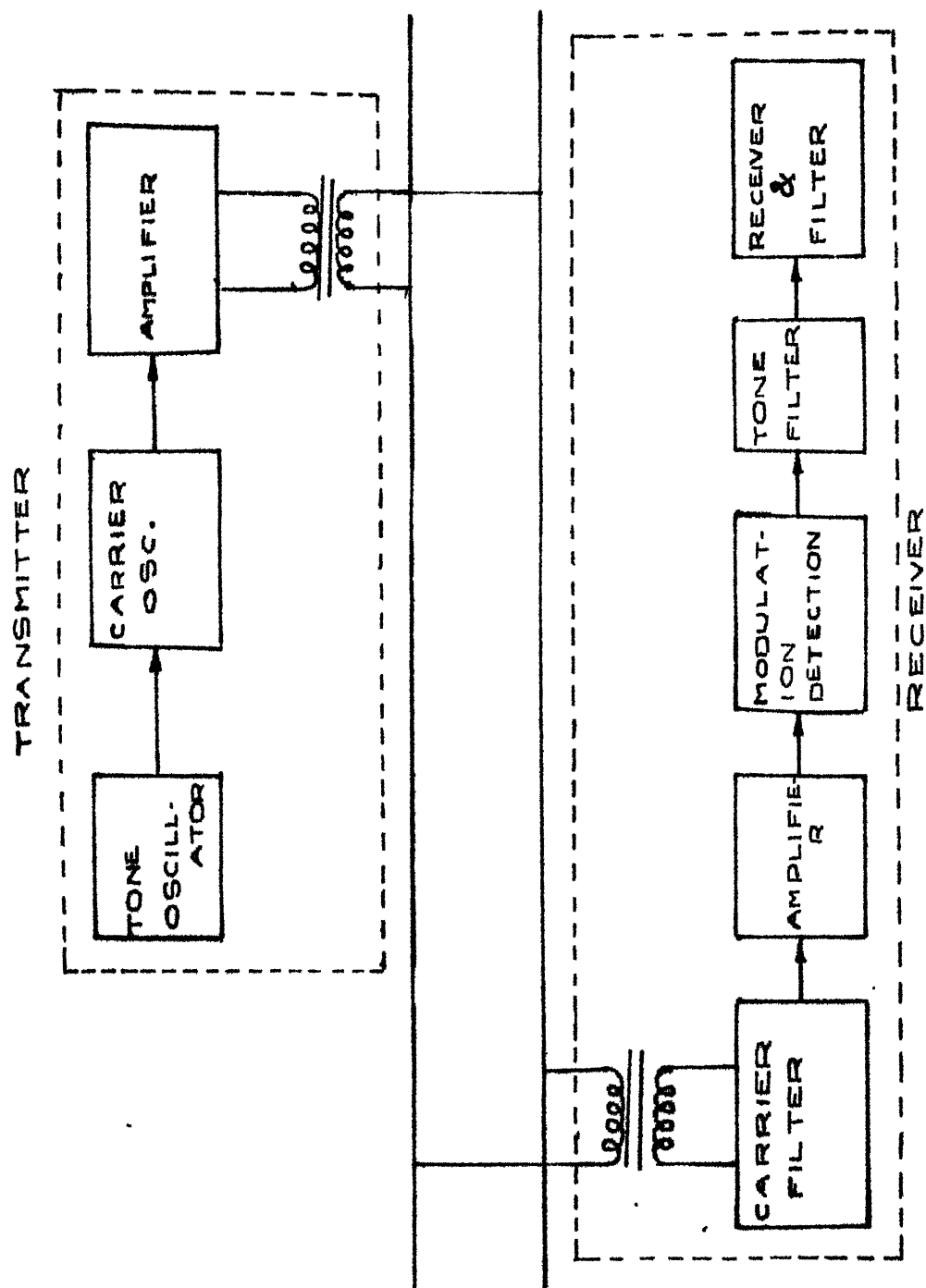


FIG 2-18 SHUNT OVERLAY TRACK CIRCUIT

Reduction of interference explained above is possible through the use of tone modulation of the transmitter carrier. Fig.2.1.6 shows a block diagram of such a transmitter and receiver.

The basic difference between the system of Fig.2.1.6 and that previously described is that the track relay is operated from the modulation signal not from the carrier. Thus interference signals, which tends to fill in the modulation, reduce the available output signal rather than enhance it.

The designer must follow the following guidelines in the choice of carrier and modulation frequencies in order to further protect the system.

1. Use non-harmonically related carrier frequencies.
2. Use non-harmonically related tone frequencies.
3. Use tone and carrier frequencies that are not close to or harmonically related to cab signalling, propulsion or public utility frequencies.

## 2.2 HOTBOX DETECTION SYSTEMS

### 2.2.1 General Information

Any bearing which departs markedly from the operating characteristics of other bearings in its class on a given [5],[1] train is a hotbox and remedial measures must be taken. In general, the cause for hotbox is the breakdown of lubrication.

The rate of journal temperature variation depends upon the nature of the defect, the loading, the speed of the train etc. One can seldom pinpoint where a hotbox had its origin or how long it will run in an overheated condition before burn-off conditions prevail.

Because an overheated bearing can take one of many paths to the critical stages of destruction, time becomes the most important parameter in the detection process. The journal being obscured from view in its enclosure, can only give evidence of its condition indirectly. For the thermal flux to heat the external box surfaces, the thermal impedance of the assembly (brass, wedge and box) must be overcome. The expression for the thermal circuit of the journal assembly may be given by  $T = \phi \times R$  where  $T$  is the temperature difference between the heat producing surface, and the external surfaces of the housing;  $\phi$  is the thermal flux and  $R$  the resistance or impedance offered to the flow of heat.

For all practical purposes the statement serves to point out that the temperature difference between the bearing surface temperature and outside box temperature can be very high depending upon the value of  $R$ , the thermal impedance. The value of  $R$  depends broadly on the conductivity and mass of the material carrying the heat-flux, if the mass is large and conductivity is poor, a large temperature difference exists, and a large time is required for external surface to reach a



given temperature. It is obvious, that the temperature of the outside box surface is a function of time if a journal box is in the process of overheating.

A normal bearing will achieve an equilibrium, a steady state temperature, after several hours of running. That is, a heat balance will be obtained and the running temperature will be stabilized. The heat being generated will be exactly balanced by the heat loss of the system. Consequently, the temperature can rise no further unless a defect causes more heat to be generated. If the defect is so severe as to cause the generation of so much heat that the temperature equilibrium point lies above the destruction temperature of the bearing burn-off condition will obtain and unless detected in time, a derailment accident is certain. The difference between normal bearing and the hotbox is that the normal bearing is in a steady-state condition and hotbox is in what is known as a transient condition.

Investigations have shown that the mean temperature for a large number of normal bearings (solid type) is  $130^{\circ}\text{F}$  above ambient temperature. The individual journal temperature will be in a band from  $110^{\circ}\text{F}$  to  $150^{\circ}\text{F}$ , above ambient. These slight variances from the mean temperature are caused by a wide variety of conditions such as, loading, bearing size, bearing contact surfaces, clearances, etc.

The investigations indicated that the normal box mean temperature on the vertical surfaces is about  $30^{\circ}\text{F}$  above ambient. This indicates that above  $100^{\circ}\text{F}$  exists between bearing and outer surfaces of the journal assembly under steady state conditions. Most of this temperature drop exists at the interfaces between the brass and wedges, and the wedges and the top of the box.

About fifteen minutes must elapse between the time that a change takes place at the journal-bearing interface and the time that the box surfaces begin to respond to change. Before a significant detectable change takes place at the hotbox surface at least half an hour must elapse. The temperature of the journal box cannot give an indication about seriousness of hotbox, because higher indication may have been a hotbox that has been developing slowly and running for hours at elevated temperatures. That box with the lower indication may have had a severe defect causing the journal temperature to rise rapidly but not having sufficient time elapse to heat up external surface before passing over the detector. It remains that it is sufficient to indicate that the box is in a transient condition.

The radiated energy from the target (journal box) is not directly proportional to the temperature in degrees Fahrenheit, but rather to the fourth power of the absolute temperature.

Another factor which can influence the energy radiated from the journal box is emissivity. It is fortunate that most boxes exhibit like characteristics in radiating energy. Occasionally a box may be newly painted or be covered with cement dust. These conditions would change the surface properties of the journal. Because of these few uncontrolled variables, a temperature measurement is a difficult process. It is a qualitative rather than quantitative analysis that hotbox detector system performs.

#### 2.2.2 Hotbox Transducers

In the past, the manifestations of an overheated bearings were readily indicated by sight (smoke or flame), sound (screeching) or smell (unmistakable odor). Personnel stationed at frequent intervals along the right of way were able to recognise these signs often enough to prevent serious derailments.

With the advent of more efficient technology, hotboxes are detected with the help of what is known as infrared hotbox detector. An infrared hotbox detector is a device which is concerned with infrared energy emitted by the journal box. It is essential that the detector be responsive to the particular wavelength of radiation which the journal box emits. To eliminate extraneous heat sources from the detector the view of the scanner will be blocked with a shutter and allow it to open

long enough to see the target. As added insurance the sensor and the optical material should be chosen which responds greatest to the specific type of radiation given off by the target. The wavelength of electromagnetic energy emitted by the target will be approximately 7 to 15 microns.

Germanium is used for optical system to respond to the spectral region we are concerned about. Earlier, light or audio alarm was used to indicate that train has produced at least one abnormal indication. The principle of detecting a hotbox with infrared hotbox detector remain unchanged. Detailed description of infrared hotbox detector is given in Chapter 4.

## CHAPTER 3

### AXLE COUNTING SYSTEM

Axle counting is a recent scheme of signalling that counts in and counts out the axles when train enters and leaves the track section and gives a 'CLEAR' indication when the count equals; otherwise it gives an 'ENGAGED' signal. It is superior to the conventional signalling schemes described in Chapter 2, because of the following reasons :

1. It's performance will not be affected by ballast resistances.
2. It is a noncontact type, so it will not need insulated track sections, which indirectly reduces the need for continuous maintenance and supervision.
3. Since this works on the principle of tone modulation, interference by distortion products is negligible.
4. The presence of oil and grease on the rails, unlike in the case of dc track circuit will not affect the performance of transducers.

In axle counting system, the axles of the train when passing over the transducers modulate the normal 5 KHz signals of the receiver to form a dip. The signals after amplification are fed on the transmission lines to the indoor equipment which

processes and evaluates the received signals. For two detection point axle counting system (normal main track without any crossovers), four amplitude modulated sinewave signals are converted into digital pulses and these pulses are counted in or counted out depending on the condition that these pulses correspond to the train moving into the track section or leaving the track section.

### 3.1 DETAILS OF THE TRACK TRANSDUCERS

To monitor a track section, the outdoor equipment is provided at two ends of the section. The equipment at each end consists of

1. Two sets of track transducers, each consisting of :
  - a. Transmitter coil in a composite aluminium fibre glass housing
  - b. Receiver coil in a composite aluminium fibre glass housing
  - c. Base clamp fitted on to the bottom flange of rail for mounting the transmitter and receiver housings.
2. Electronic junction equipment consisting of :
  - a. Oscillator, generating 5 KHz signals feeding two transmitter coils of both track transducers connected in series
  - b. Two numbers of receiver amplifiers for amplification of the signals independently received from two receiver coils of track transducers.

The output of the receiver amplifiers is connected to the cables for onward transmission to indoor equipment.

While the transmitter housing is fixed on the base clamp on the outer side of the rail, the receiver housing is fixed on the inner side. Transmitter coils are energized by the common oscillator. The arrangements and shape of transmitter and receiver coils are such that the two magnetic fluxes generated in the vicinity of the rail and these two fluxes traverse receiver coil in opposite directions.

Reluctance of the magnetic path of the two fluxes is different under normal conditions when no wheel passes on the track transducers. One of these two fluxes is quite large compared to the other and the resultant flux induces a voltage in the receiver coil. When the wheel passes over the track transducers the screening effect of the wheel flange causes a reduction of the larger flux to a value nearly equal in magnitude to that of the other. These two fluxes cancel each other and the induced voltage in the receiver coil falls to a low value.

The ratio of these two fluxes can be adjusted with suitable initial adjustment by rotating the transmitter coil inside the housing assembly. This adjustment depends on the profiles of different rail sections in use.

The track transducers are fitted in the staggered position on the rails of the track. Each transducer coil therefore detects signals which are displaced in time. It is only this time staggering of these signals that gives direction of the train.

The track signals received from the receiver coils of the two track transducers fed independently to a two stage tuned amplifier circuit. The tuned frequency is 5 KHz with a 3 dB bandwidth of  $\pm 250$  Hz. Any noise picked up by transducers in receiver area being a low frequency is suppressed in the receiver amplifier and only 5 KHz signal is transmitted through the cable to the indoor equipment. For proper performance, the output impedance of the amplifier should match the cable impedance.

### 3.2 INDOOR EQUIPMENT

The track signals may be from an outdoor equipment very near to the indoor equipment or as far as 12 km. Hence, attenuator pads are provided to adjust the signal level to the next section. The attenuators are adjusted so that the input level to the next section is 500 mV peak to peak. The high pass filter filters out 50 Hz and its harmonics and passes the desired 5 KHz signal. This signal is amplified, rectified and fed to lowpassfilter which filters out 5 KHz signals and gives the modulating signal representing wheel dips. This



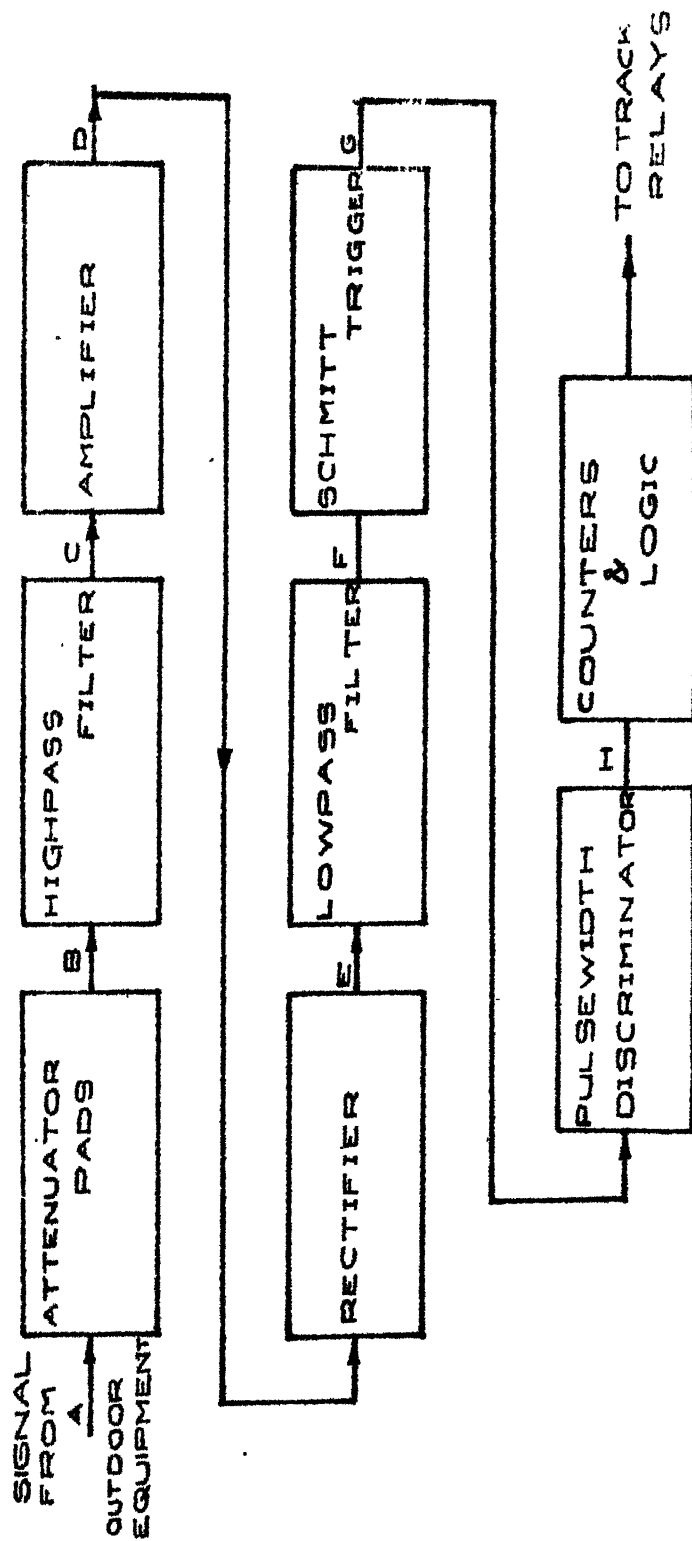


FIG.31 INDOOREQUIPMENT

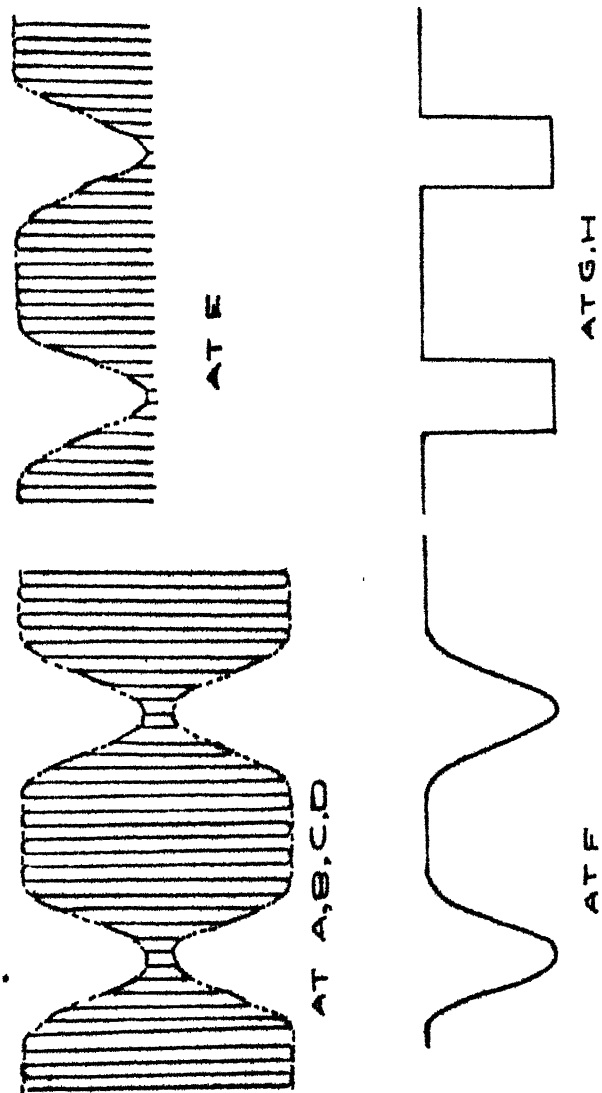


FIG.3.2 WAVEFORMS AT VARIOUS POINTS OF THE  
INDOOR-EQUIPMENT

demodulated signal is converted into pulses by Schmitt trigger. The pulse width generated by normal train axles is always greater than 7 ms even at a train speeds of 200 kmph. Any pulse less than 5 milliseconds duration therefore represents the noise induced in the system due to extraneous sources. The pulsewidth discriminator cuts out the pulse having a pulse width less than 5 milliseconds and passes other pulses to the counters. For a two detection point axle counting system four similar types of pulses staggered in time are fed to the counters. The counters and logic counts in or counts out the pulses depending on the movement of the train on the track section. Logic involved is explained in Chapter 4 in detail in conjunction with proposed system. The logic will take care of all types of train movements (shunting and through running). Typical waveforms at each input block of Fig. 3.1 is shown in Fig. 3.2. A better signal processing scheme is suggested in Chapter 5.

## CHAPTER 4

## INFRARED HOTBOX DETECTOR

In this chapter the principle of operation of the infrared hotbox detection system is explained in detail. An infrared hotbox detector is a device which is concerned with infrared energy emitted by the journal box.

In a basic arrangement for a bidirectional system with single junction box, figure 4.1a, or multiple junction boxes, fig. 4.1b, magnetic wheel detectors on both approaches to the scanner location initiate system operation. The track [2] mounted equipment for a single junction box system consists of two mounting assemblies (scanner and blower), four wheel detectors, a junction box, and connecting cables.

A basic unidirectional system does not require wheel detectors 2 and 4, fig. 4.1a or 4.1b and a directional relay printed circuit board. An optional reverse direction lockout features may be available to avoid scanning in the reverse direction.

## 4.1 BASIC OPERATION

A train approaching the scanner location turns on the system when it passes over the advance wheel detector, figs. 4.1a or 4.1b. A control pulse generated by the wheel opens the scanner door and starts the pen recorder.

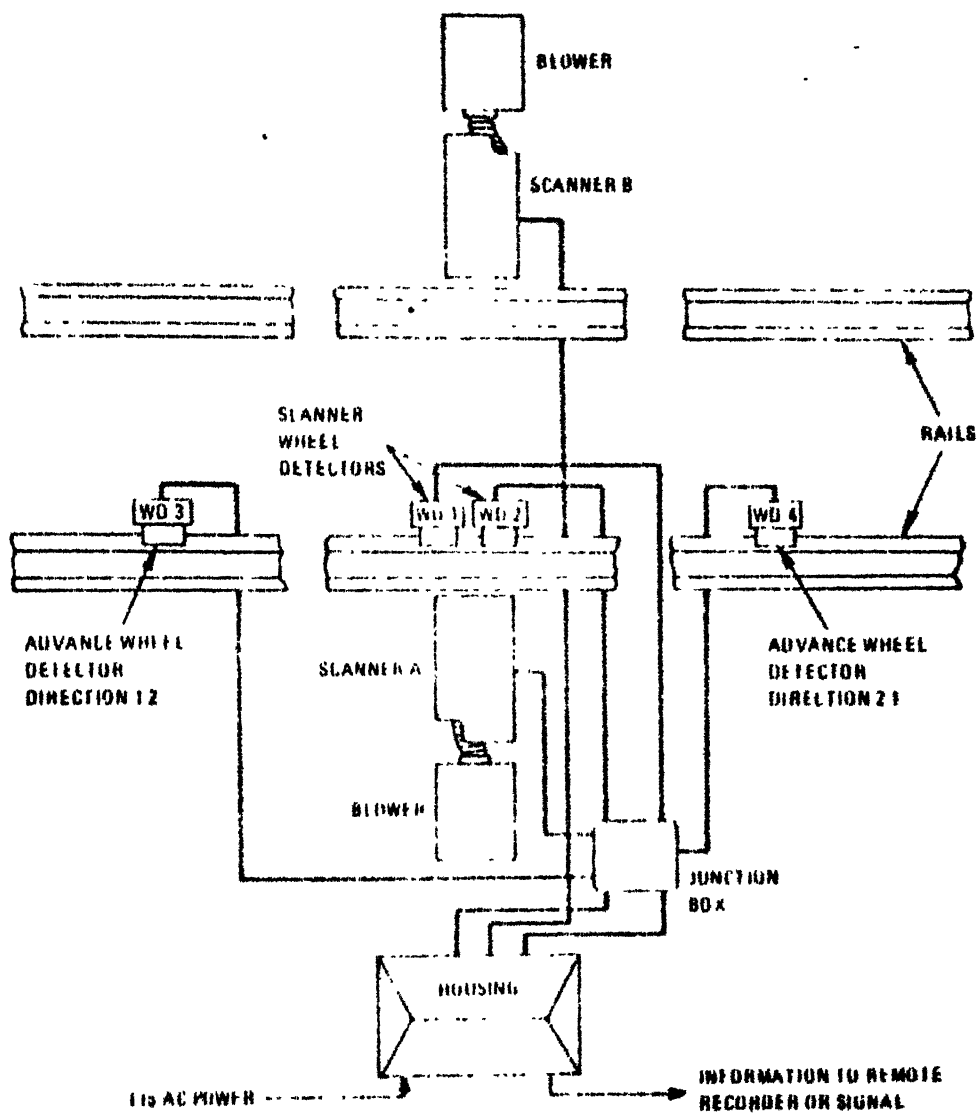


Figure 4-10 Basic arrangement of a bidirectional system - single-junction box arrangement for systems manufactured after 1974.

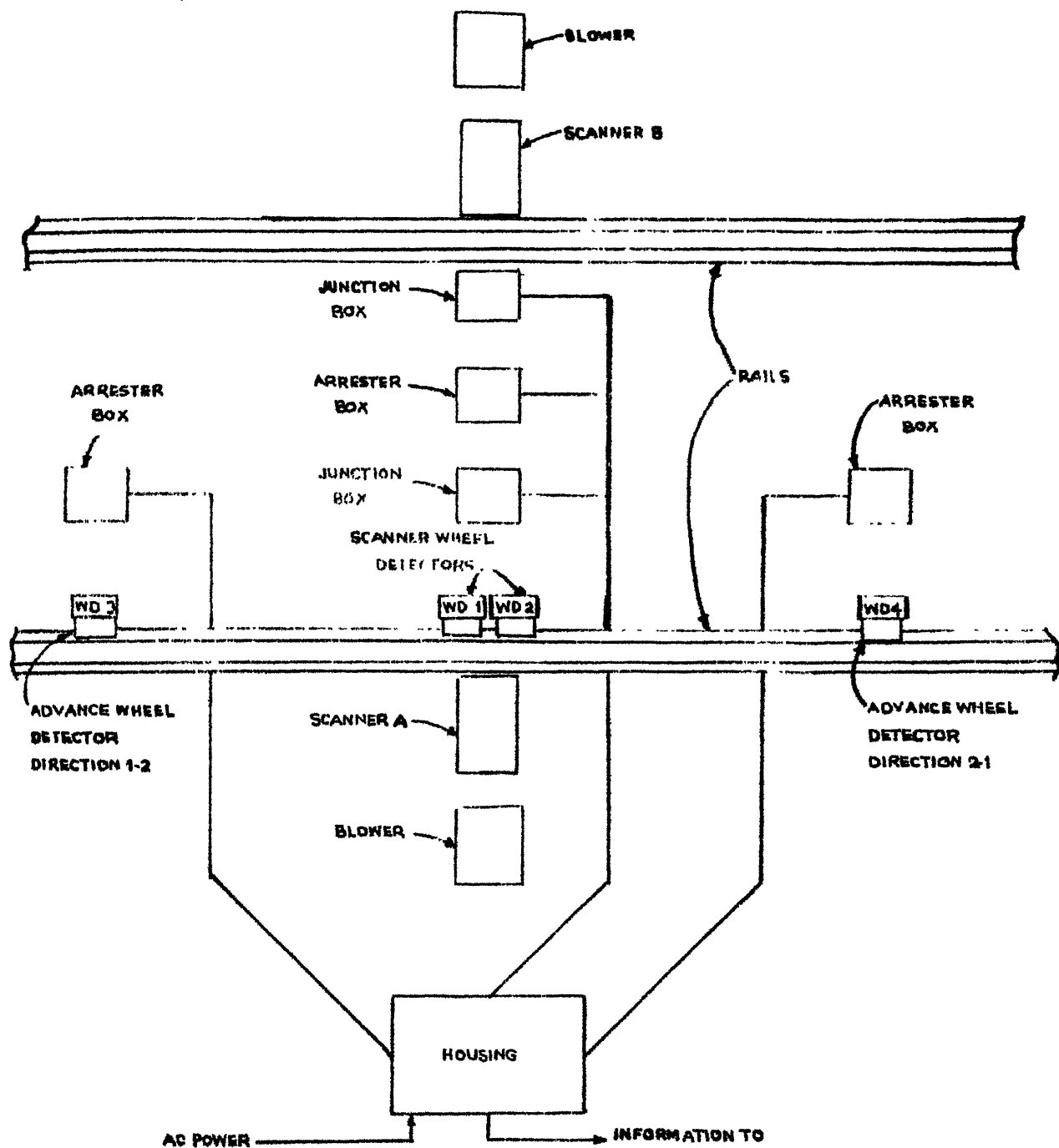


Fig 4-1b. Basic arrangement of a bidirectional system

The passage of each wheel over the scanner wheel detector results in a pulse that is processed by the gate generator and amplifier gate units located in the way side housing. The output ultimately operates the optical shutter in the radiometer (located in the scanner) to briefly expose a small infrared detector. Radiated infrared energy from the passing journal is collected and focussed on the detector which produces a current proportional to the total amount of collected infrared energy. The current is converted to a voltage and amplified in the radiometer. This voltage pulse is fed to the amplifier gate unit to drive pen recorder.

After scanning the last journal, a timing network on the gate generator unit allows 14 seconds to elapse, and then closes the scanner door. About 1.5 seconds later a check pulse causes the radiometer to view a reference target on the inside of the scanner door to determine that the system is functioning properly. The system now reverts to a standby mode during which system sensitivity is automatically checked and adjusted in every minute.

#### 4.2 SCANNER

The radiometer is mounted at an angle in the bottom of the scanner case, Fig. 4.2, so that its window is protected from snow, dirt, etc. A front surface mirror, also mounted in the bottom of the scanner case, is made of chromium-plated brass which is polished on both sides. Should it become

scratched after several years use, it can be turned over. The 2 watt mirror heater is continuously energized from the 24 volt dc supply.

The radiometer is hermetically sealed to prevent the entry of dirt and moisture.

The detector, a one millimeter square metallic crystal, changes its resistance when exposed to infrared radiation - it is photoconductive. A thin layer of vapor deposited metal on the surface of the detector reflects visible light but allows heat to pass.

The detector is accurately located at the focus of a precise system of flat and parabolic front surface mirrors. This optical system focuses a beam of heat from a  $\frac{1}{2}$  inch square spot on the wheel hub through the open scanner door to the chrome mirror in the bottom of the scanner case, thence to the parabolic mirror in the radiometer, the flat mirror on the inner side of the radiometer window, and to the infrared detector.

The shutter normally interrupts the beam of heat to prevent undesired stray infrared radiation from striking the detector. The passage of a wheel over the scanner wheel detector generates a gating pulse which rotates the shutter to expose the detector at the precise instant the wheel hub comes into the field view. The shutter is open only a few



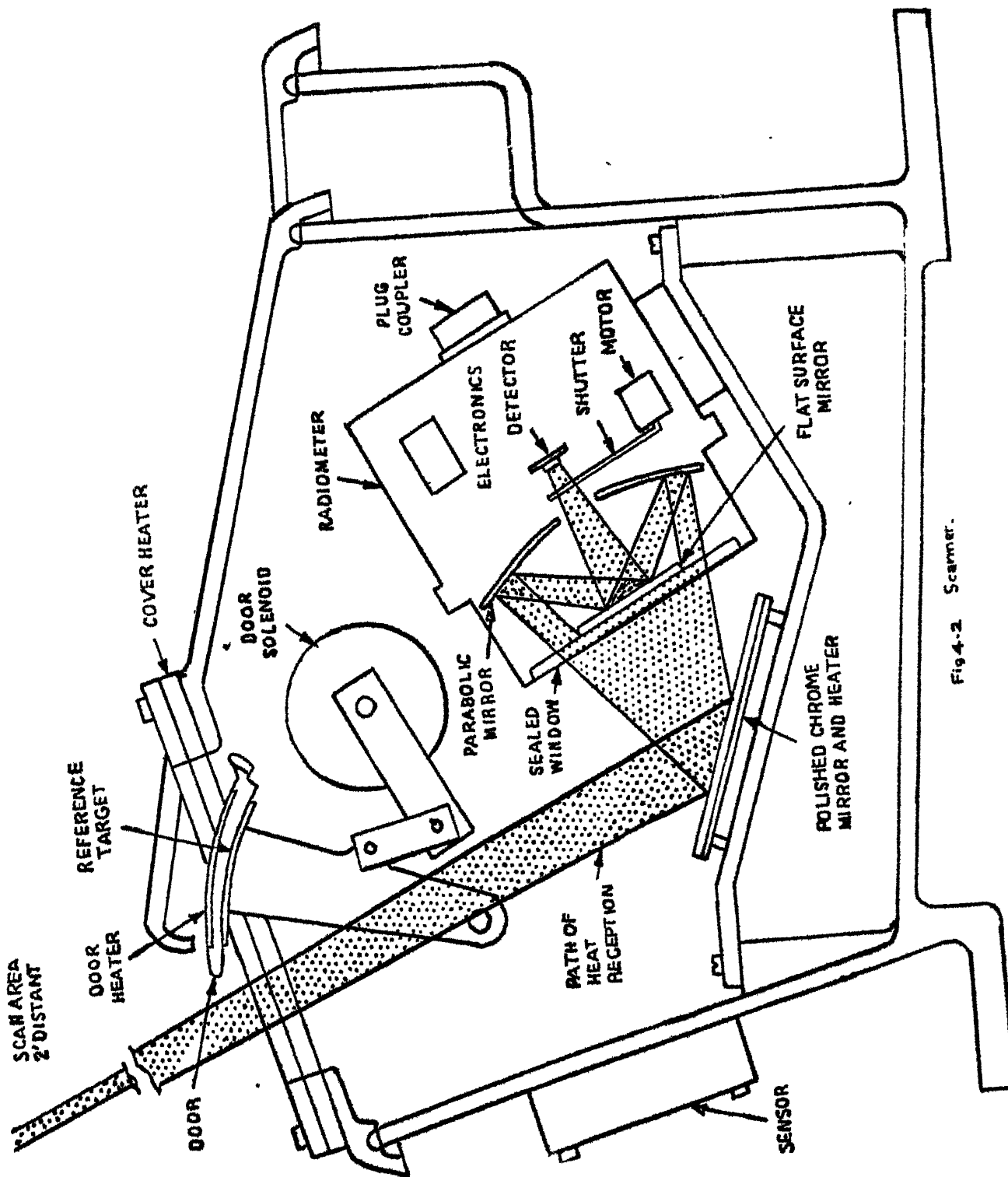


Fig 4-2 Scanner.

milliseconds, thus establishing the length of the heat pulse generated by the detector. The heat pulse is amplified in a high-gain preamplifier, located in the radiometer, and fed to a line driver.

#### 4.2.1 Door and Cover

The door located in the scanner cover, Fig. 4.2, is opened by a rotory solenoid and closed by a spring and counterbalance weight. The solenoid is connected to the door by a dead center mechanism which locks the door to discourage vandalism. The return spring is not effective as the door starts to open, thus the full power of solenoid is able to set the door in motion and fully stretch the spring at the open position. When energy is removed from the solenoid, the spring quickly closes the door. The 20 watts heater on the door melts accumulated snow.

#### 4.2.2 Reference Target and Sensor

The reference target, Fig. 4.2, a heater mounted on the underside of the door, and the sensor, attached to the front of the scanner case, are parts of the systems self calibration feature.

#### 4.2.3 Blower

The blower is equipped with a replaceable type filter, a screen, snow baffles, and a hood. The filter should last for

several months, depending upon environment conditions.

#### 4.2.4 Wheel Detectors

The wheel detector is epoxy encapsulated magnetic device tie-mounted on the inside of the rail about 1/4th inch below the location of the wheel flange. This type of mounting eliminates the need for rail drilling and the problems of rail creepage. The magnetic structure contains permanent magnets which set up a flux field through the coil. When the wheel approaches, Fig. 4.3, the magnetic flux builds up until the wheel is exactly over the centerline of the structure and then decays as the wheel recedes. A current is generated in the coil, the action of this flux current has one polarity during flux build up and the opposite during flux decay.

The point of current reversal is accurate to wheel centre position within  $\pm 1/4$ th inch. The coil is protected from lightning damage by the arresters in the main junction box, Fig. 4.1a or by the associated arrester box, Fig. 4.1b.

#### 4.3 OPERATION

As the train approaches the scanner location, it first passes over either advance wheel detector 3 or 4, Fig. 4.1a or Fig. 4.1b. This announces the arrival and will readies the system for operation. It also establishes train direction, which is used to select the scanner wheel detector preceding the centerline of the scanner. For example, if advance wheel

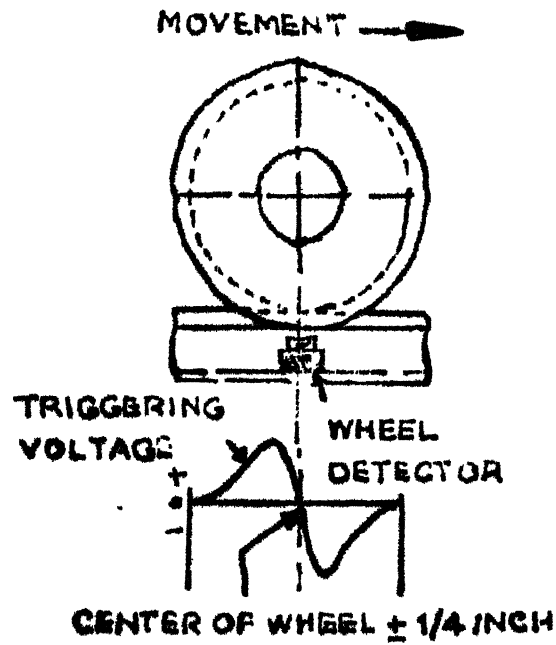


Figure 4-3.

Wheel detector output current.

detector 3 is actuated, scanner wheel detector 1 is selected. This direction is referred to as direction 1-2, with reference to the scanner wheel detectors.

The train next actuates WD1 which causes the scanner to scan the journals and convert radiated heat energy to electricity on a proportional basis. The electrical analog of the wheel heat profile is carried by cable to the housing where electronic equipment extracts the information desired.

The activation of an advance wheel detector and selected scanner wheel detector operates a 14-second timer which keeps the system in operation. When train slows and stops at the scanner installation, the timer times out and the scanner reverts to standby operation. If a track circuit relay contact is available, or if overlay transceiver is provided, the direction of train movement is retained. If, however, no track circuit information is available, the train direction is lost. For this reason, track circuits are recommended where trains may stop. When the train starts again, the first wheel over an active wheel detector reactivates the system which continues to scan the remaining wheels until last wheel passes. After 14 seconds, the system again reverts to standby operation, and when the track circuit clears the directional memory is released.

#### 4.3.1 System on Standby

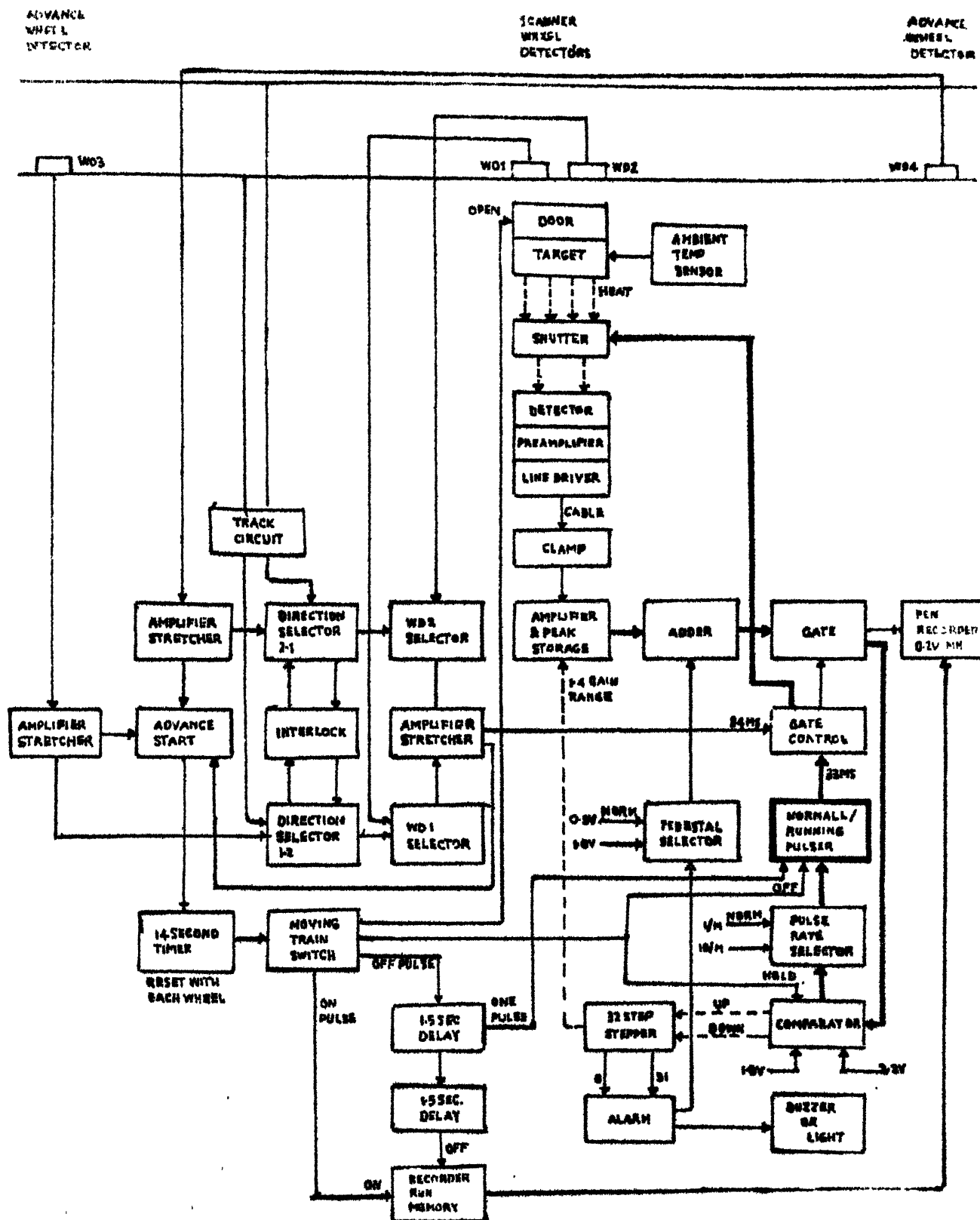
During the absence of a train, the wheel Thermo-Scanner system is on standby. Standby operation involves a self-calibration feature, which once in every minute opens the radiometer shutter. The normal optical path of the radiometer is, however, blocked by the door, which is closed during standby operation. As previously described, the target on the inside of the door is heated to a temperature above ambient which is indicative of an overheated journal (hotbox). Thus the radiometer reads the temperature of the target. In the wayside housing the amplifier gate board analyses the output voltage if it is a level other than expected from a hotbox the gain of its amplifier is changed to bring the output to the proper level. This gain is controlled by 32 step digital counter.

The heavy lines on the block diagram, Fig. 4.4, outline, this operation. Starting with the heavy lined block, the normally running pulser produces pulses once in every minute. The pulses pass through the gate control circuits and open the shutter in the radiometer. With the door closed, the radiometer reads the target temperature which is translated by the preamplifier to a potential of about 1 volt. The heat pulse is fed by the line driver in the scanner back through the cable to the test unit board in the modular equipment cabinet where an electronic circuit clamps the output pulse

after a predetermined time. The clamp circuit terminates the heat pulse about 6 ms following the opening of the shutter. The heat pulse is fed to an amplifier and a peak storage device (a capacitor with isolation circuitry). The device stores the highest voltage attained from the time the shutter is opened until the signal is clamped.

A fixed voltage pulse (called a pedestal) is added to the heat pulse. The pedestal is normally 0.5 volt in height. The combined heat pulse and pedestal is fed through a gate circuit (controlled by the same gate pulse that originated the shutter movement) to the comparator.

The comparator checks that the voltage of the combined pulse (representing a hot journal) is between 1.8 and 2.2 volts. If the voltage is not within these limits, sensing circuits within the comparator step the 32-step stepper one step in the direction required to correct the situation. The 32-step stepper controls the gain of the amplifier through which the heat pulse was fed before the peak storage. When the heat pulse is low, the comparator causes the stepper to increase the gain in the amplifier so that after one or more steps the pulse is of the expected height. This ensures that, during normal operation, heat measured from an overheated journal (at the same temperature as the target) displays a 10 mm pulse. The hot journal threshold.



**Fig. 4.4. Block diagram, bidirectional system operation.**



A supplemental comparator circuit, the pulse rate selection governs the pulse rate of the normally running pulser by increasing the rate from one per minute to ten per minute any time the comparator detects a pulse out of tolerance. This ensures prompt correction of any gain change and is especially valuable during the initial start up and test. Things which might cause a change in the heat pulse output are dirt on the optics, component aging, ambient temperature changes and faulty system alignment.

A second supplemental circuit in the 32-steps stepper is an alarm circuit. It senses when stepper has stepped either to the top or bottom of its range. The circuit then causes the pedestal selection to double the pedestal voltage. This switches on a transistor relay driver (for external alarm) to warn the person reading the tapes that the system is no longer able to compensate for whatever condition is causing the heat pulse reduction. When such a condition is corrected the comparator steps the gain back down again to get the heat pulse within tolerance. The comparator does not operate during normal system operation; just during standby.

#### 4.3.2 Train Approaches

As the train approaches the scanner site, it occupies the track circuit (if one has been provided) so the direction established when the train first actuates the advance wheel

detector is maintained during the trains presence. This may be a spare contact on an existing track relay, if such is available or it can be a series overlay.

The train after occupying the track circuit, passes over the advance wheel detector. The electrical pulse generated by the wheel detector coil is fed over a cable to the wayside housing where it is amplified and shaped by an amplifier - stretcher that picks up an interlocked relay in the direction unit board (the direction selector) to establish the train direction. The relay is held by the track circuit. The activated direction selector selects the proper wheel direction for operating scanner.

The gate generator associated with the advance wheel detector and the selected scanner wheel detector have a second output - to provide an advance start for taking the system out of standby and readying it for operation. The advance start circuit actuates a 14 second timer which is reset to zero when a wheel passes a wheel detector. The timer in turn operates a moving train relay as long as wheels keep resetting the timer and turns off 14 seconds after the last wheel pulse. While the relay is energized, a pulse is delivered to the recorder run memory which activates pen recorder. A second function of this relay is to open the scanner door, removing the calibration target from the view of the detector. A third function is to stop the normally running pulser and hold the

comparator and therefore, the 32-step stepper position it had attained at the time of the trains arrival.

The distance between the advance wheel detector and the selected scanner wheel detector must be long enough to allow the door to open, before the train reaches the scanner.

When a wheel passes the selected scanner wheel detector, the associated gate generator applies a 24 ms pulse to the gate control circuitry in the same manner as the normally running pulser did during standby operation. The gate control circuitry opens the shutter allowing a detector to view the passing wheel hub, which has in the meantime moved into view. The heat received during the wheel scan is converted into electrical energy in the same manner as described under standby operation. The heat pulse is gated, amplified, stored, stretched, and added to the pen recorder where it is displayed.

#### 4.3.3 Train Leaves

When the last wheel passes over the trailing advance wheel detector, the 14-second timer receives its last pulse. 14-seconds later, the timer turns off the moving train switch which closes the scanner door, thus interposing the calibration target in the detector field of view. The off pulse of the moving train switch starts a second timer which,  $1\frac{1}{2}$  seconds later (to give the door time to close) puts a single pulse into the pulser to open the shutter in the usual way. One and a half seconds after

the second timer operates, a third timer operates which turns off the recorder run memory. The action is the same for a train that slows and stops.

Following the scanner shutdown, calibration pulse, and recorders shutdown, the train eventually clears the track circuit. When it does, the directional memory is dropped and the system is ready once more to accept a train from either direction. The system is now in standby and returns to its self-compensating function.

## CHAPTER 5

### PROPOSED SYSTEM

The proposed system takes care of the signals that come from both hotbox detector and axle counter transducers and gives appropriate indication after processing them. The software that takes care of both functions of hotbox detection and axle counting is developed for M6800 based system and tested by simulating real time signals using a toy train. This chapter gives detailed description of the specifications of the proposed system, how they are proposed to be met and the approach taken in the development of the software.

#### 5.1 SIGNALLING SCHEME

##### 5.1.1 Specifications

The specifications that are typical are given below :

1. The track mounted electronic detection equipment shall be non-contact type and will not infringe the standard moving dimensions. It shall consist of a suitable transmitter and receiver with an electronic junction box. The transmitter is to give an output at  $5 \text{ KHz} \pm 15 \text{ Hz}$  frequency. It shall electronically sense the passage of wheels and transmit modulated signal at  $5 \text{ KHz} \pm 15 \text{ Hz}$  and shall be actuated by wheel flanges and not by other parts of the train (rail brakes, toilet pipes, suspended clamps etc) and its operation

shall be independent of

- a) the type and condition of the wheels such as diameter, design of wheel, wear and tear permitted,
  - b) the type of rail section and construction such as welded or non-welded rails and
  - c) the type of traction such as electronic, diesel or steam and the weight of rolling stock.
2. The information generated by the track detection equipment shall be processed by a microprocessor based system.
  3. The equipment shall count in or count out the axles at every end of the nominated track section depending upon the direction of the train.
  4. The equipment should be capable of being connected with four detection points simultaneously with one processor.
  5. The operation of the equipment shall be fully reliable at all train speeds in the range of '0' to 200 km per hr. The equipment shall ensure that until all the axles that enter a section are completely counted out, the section concerned shall not be shown as clear.
  6. The equipment shall be capable of simultaneously counting in and counting out, that is simultaneous counting in and counting out of the pulses from any end shall not interfere with each other.
  7. The equipment shall not be susceptible to operation by maintenance tools at or near the track equipment.

8. The equipment shall be insensitive to extraneous magnetic or electrical fields (such as due to traction return currents or electrified traction motor fields, vehicle magnets for induction train control, wheels with residual magnetism etc., or due to any other sources).
9. Detecting equipment at a junction of two consecutive sections shall be able to control separate processors for each section, i.e., each detection point should be capable of being fed to two systems.

To meet the above mentioned specifications axle counting scheme is chosen because of the advantages mentioned in Chapter 3. The software developed assumes that the processed signals are available to take the necessary decision. The following scheme is suggested for processing the signals available at the input of the indoor equipment.

#### 5.1.2 Proposed Signal Processing Scheme for Axle Counting

Proposed signal processing of each output of the track transducer is given schematically in Fig. 5.1. This uses coherent demodulation of AM signal available at the indoor equipment. In this coherent demodulation PLL is used for tracking the carrier signal.

A major advantage of proposing PLL based coherent AM demodulation is that it track the 5 KHz signal even the oscillator drifts, due to various environmental conditions.

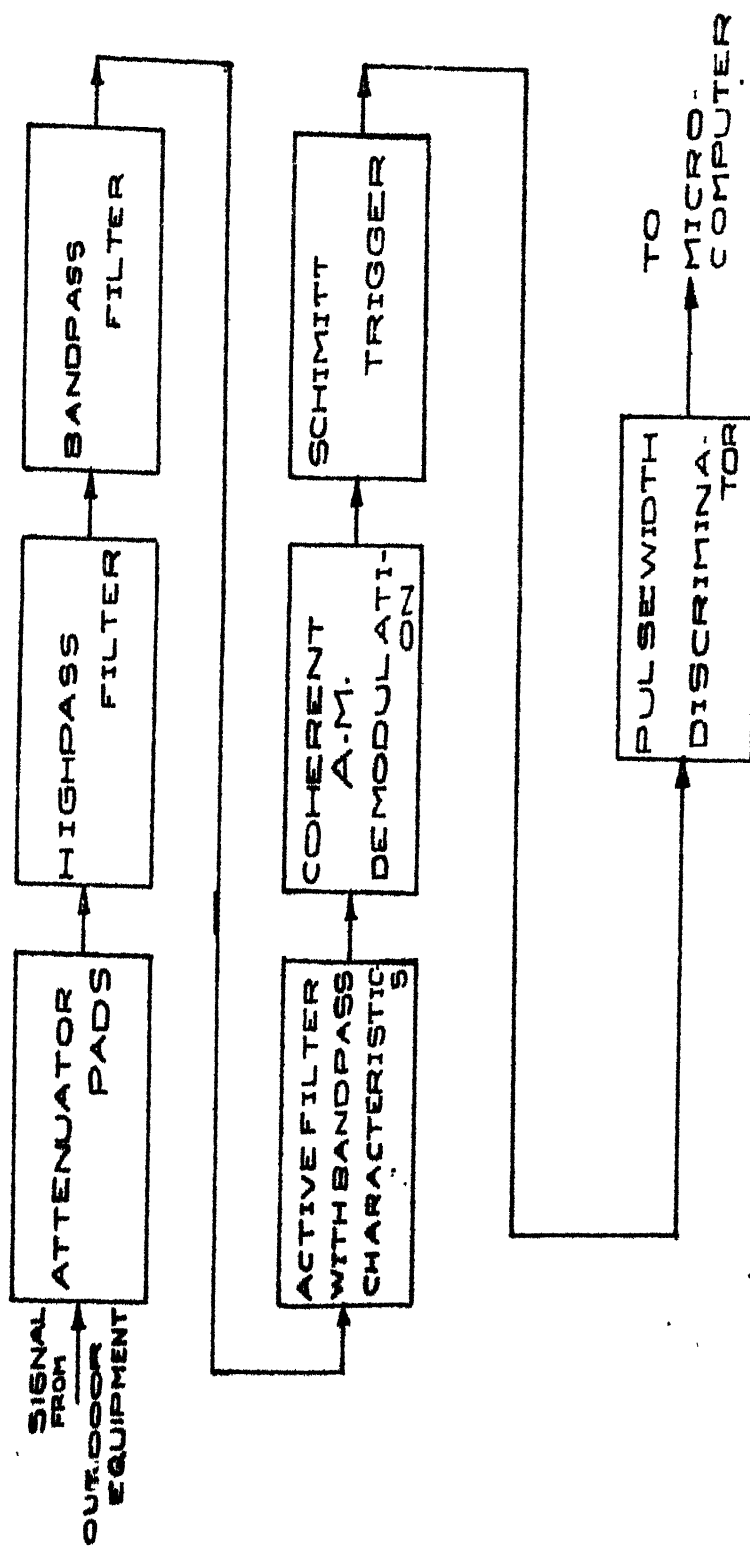


FIG. 5-1. PROPOSED SIGNAL PROCESSING SCHEME



### 5.1.3 Basic Approach Involved in Axle Counting

Fig. 5.2 shows a length of track monitored with one pair of transducers at one end. The relative positions of the transitions with respect to each other of the waveforms A and B, which are the outputs of the transducers A and B respectively contain the complete information regarding the movement of an axle across the transducer - pair and the direction.

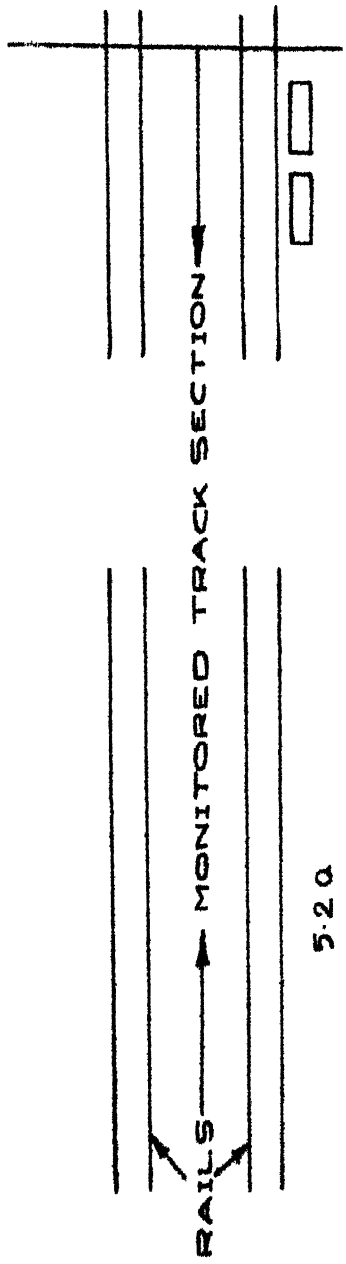
Eight unique events are shown corresponding to a transition on one waveform and a level in the other waveform, in Tables of Fig. 5.2. These events are labelled IN1, IN2, OUT1, OUT2.

The system must identify two types of train movements on the track - through running and shunting. Four cases are enumerated below corresponding to shunting and through running. The sequence of events that would occur in the waveforms A and B are given in Fig. 5.2.

(Case 1) : Only one track transducer is affected by the wheel (Fig. 5.3a).

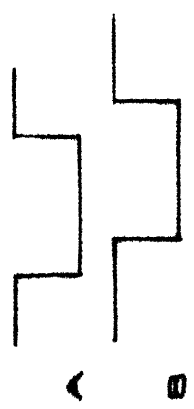
partial shunting (Case 2) : The signal of track transducer

'A' is dipped first and this is followed by 'B'. The wheel now draws back, clearing transducer 'B' first and finally transducer 'A' is also cleared. This corresponds to shunting movement into the track section and back without getting fully into



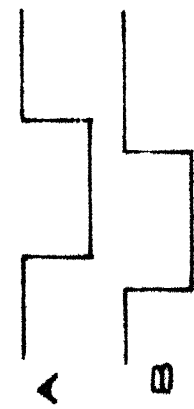
5-2a

A	B	COUNT TO BE INCREMENTED
↑	H	IN1
↓	↑	IN2
↑	L	IN1
↓	↓	IN2



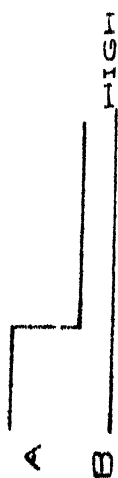
5-2b INDICATION FOR TRAIN ENTERING

A	B	COUNT TO BE INCREMENTED
↑	L	OUT1
↓	↑	OUT2
↑	H	OUT1
↓	↓	OUT2



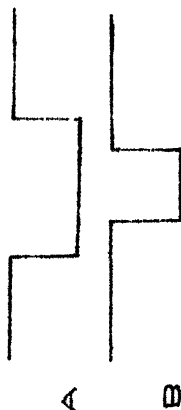
5-2c INDICATION FOR TRAIN LEAVING

IN1	IN2	OUT1	OUT2	SIGNAL
1	-	-	-	ENGAGE D



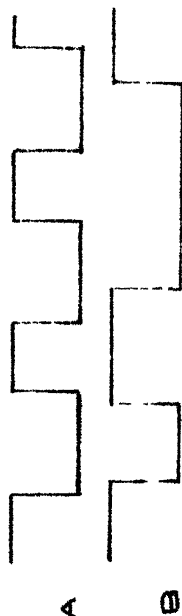
53a

IN1	IN2	OUT1	OUT2	SIGNAL
1	1	1	1	CLEAR



53b PARTIAL SHUNTING

IN1	IN2	OUT1	OUT2	SIGNAL
1+1-1	1+1	1+1+1	1+1	CLEAR



53c SHUNTING

FIG. 53 VARIOUS TRAIN MOVEMENTS

Shunting (Case 3) : The above movement is continued further than case 2 to clear transducer 'A' but not 'B'. The wheel now moves back in opposite direction reoccupying 'A' and finally clears both 'A' and 'B'. This is the case of shunting (Fig. 5.3c).

Through running (Case 4) : Both A and B are occupied and cleared successively.

The status of the track, CLEAR or ENGAGED, is indicated based on the number of occurrences of the events IN1, IN2, OUT1, OUT2; when IN1 equals OUT1 and IN2 equals OUT2 CLEAR signal is given, otherwise ENGAGED signal is given.

## 5.2 HOTBOX DETECTION

A conventional infrared hotbox detector is proposed. The output of the detector is transmitted to the indoor equipment when this signal exceeds a pre-set threshold, an indication is given to the microcomputer. The microcomputer then having been interrupted announces the occurrence of a hotbox and indicates the number of the axle to which it corresponds.

Certain assumptions are made in the implementation of the software for the hotbox detection system. These are given below along with the proposed layout of the transducers.

### 5.2.1 Assumptions

Since both the hotbox detection system and the axle

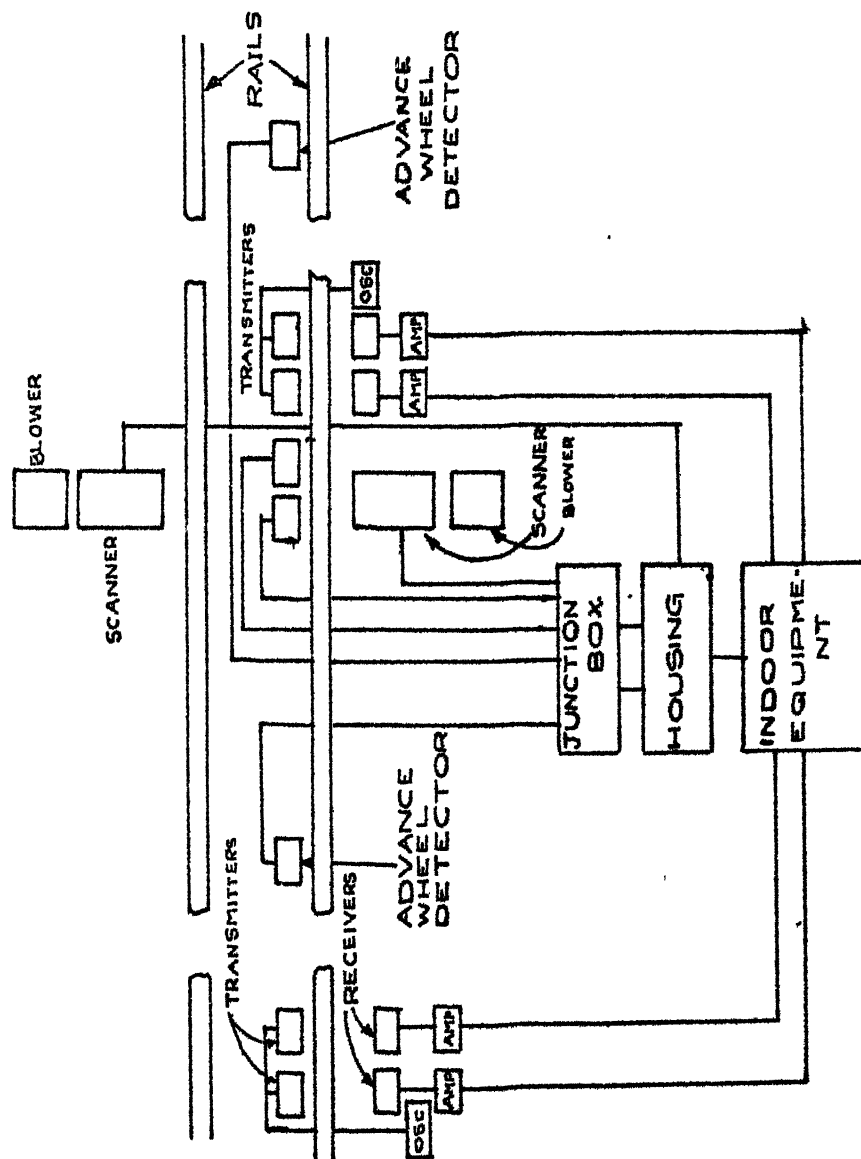


FIG 5.4 PROPOSED LAYOUT OF THE TRANSDUCERS

counting system are implemented through the same software, the following assumptions are made in the implementation of the hotbox detection system.

1. Hot axle transducers are kept at one end of track that is maintained for axle counting system, it is sufficient to detect the hotbox at one end.
2. Hot axles are detected for through running only. It is expected that a hotbox does not occur for trains in shunting as they move very slowly.
3. It is assumed that hotbox detector is placed by the side of the axle counting transducer pair.

#### 5.2.2 Proposed Layout

A proposed layout of the axle counting transducers and the hotbox detector corresponding to a section of the track is shown schematically in Fig. 5.4.

## CHAPTER 6

## SOFTWARE DETAILS

Software is developed for a combined system of axle counting and hotbox detection. The software is developed for Motorola 6800 microprocessor based system. Although any other microprocessor can meet the requirements, M6800 is chosen because of the availability of its software development system. The developed software takes care of four detection point , axel counting system. The system provides a visual information of the movement of a train on the track at a remote location, say the control room.

From the schematic diagram of Fig. 6.1 it is seen that eight processed signals from four axle counting transducer pairs are given to the logic that generates a pulse whenever a change occurs in the status of the transducer outputs. This pulse is given to one of the interrupt pins of the Peripheral Interface Adapter (PIA), that is programmed for a high to low transition to produce an interrupt to the Microprocessor Unit (MPU). The output from hotbox ax detector and lock indicator output are given to another pair of interrupt pins of the PIA. Whenever, an interrupt is recognised MPU checks the source of the interrupt and processes it as described in the subsequent sections of this chapter.

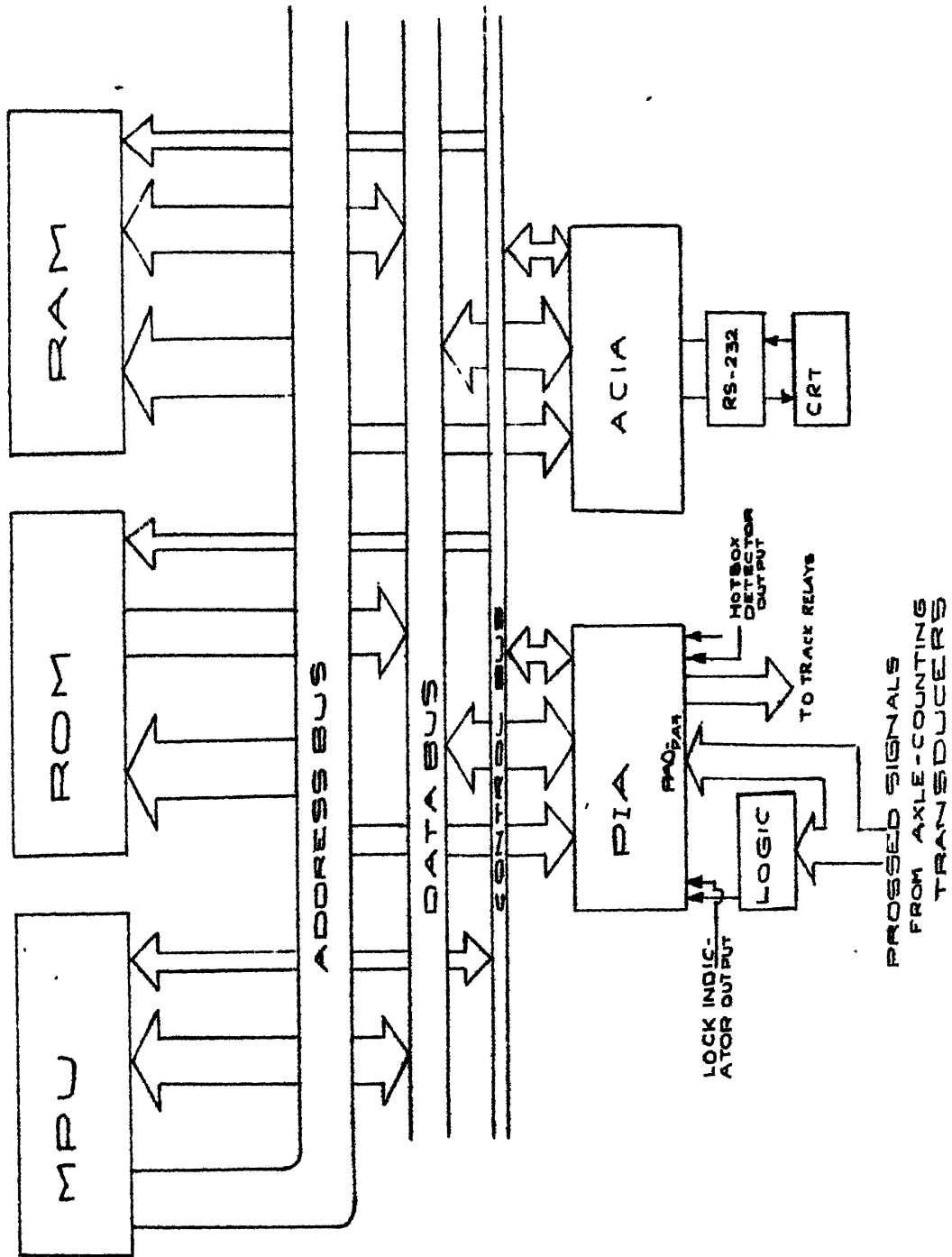


FIG. 61 SCHEMATIC DIAGRAM OF THE MICRO-COMPUTER



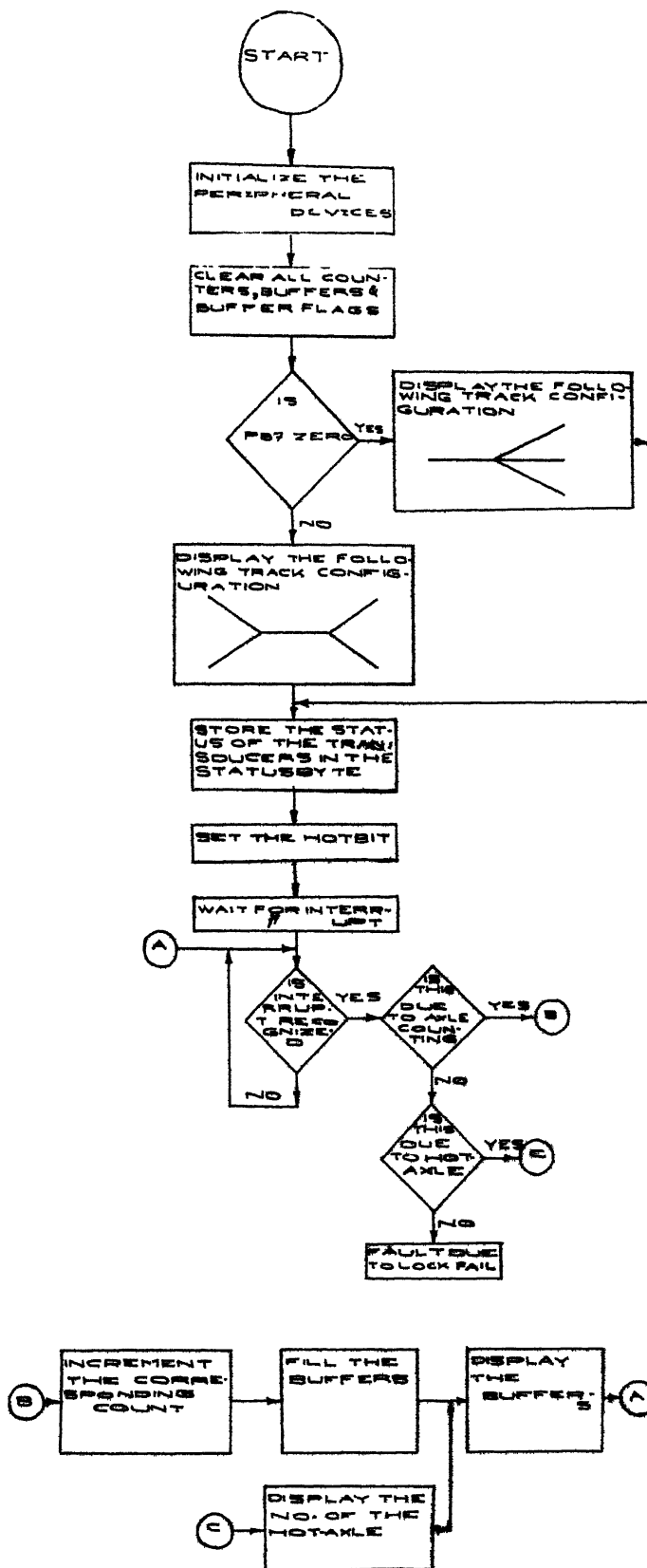


FIG. 62 MAIN FLOW-CHART

A brief flow chart of the developed software is given in Fig. 6.2. At the outset, the system initializes the peripherals, and clears the buffers and the counters. Then the appropriate track configuration is displayed with a message 'TRACK IS CLEARED'. Afterwards the MPU waits for an interrupt. If an interrupt is recognised, it checks for the source of the interrupt, and goes to the appropriate routine depending upon the source of the interrupt and does the necessary action as described in the subsequent sections. Then, it goes to the display routine whenever there is no interrupt and starts displaying the contents of the buffer. During display, if an interrupt is recognized it attends to the interrupt routine, storing the present status and then comes back to the original display routine with the help of the stored status. The detailed discussion is given in the subsequent sections.

## 6.1 INITIALIZATION

In the initialization-routine, PIA is initialized depending on the requirements on the inputs available and outputs required.

The M6800 PIA provides a flexible method of connecting byte-oriented peripherals to the MPU. The PIA, while relatively complex itself, permits the MPU to handle a wide variety of equipment types with minimum additional logic and simple programming. An Input/Output Diagram of the MC6820 is shown in Fig. 6.3.

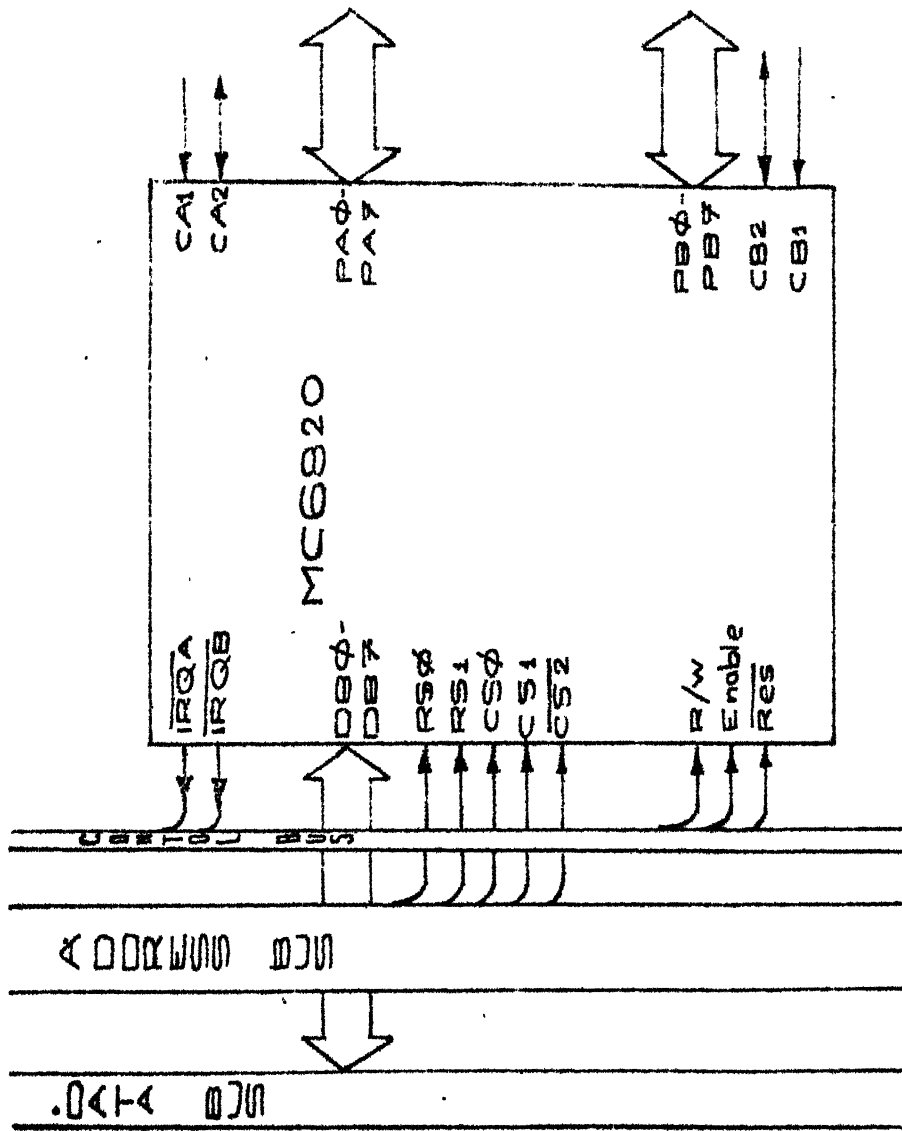


FIG. 6-3 MC 6820 PIA I/C DIAGRAM

Data flows between the MPU and the PIA on the System Data Bus via eight bi-directional data lines D0 through D7. The direction of data flow is controlled by the MPU via the Read/Write input to the PIA.

The 'MPU side' of the PIA also includes three chip select lines, CS0, CS1 and CS2, for selecting a particular PIA. Two addressing inputs RS0 and RS1, are used in conjunction with a control bit with the PIA for selecting specific registers in the PIA. The MPU can read or write into the PIA's internal registers by addressing the PIA via the system Address Bus, using these five input lines and the R/W signal. From the MPU's point of view each PIA is simply four memory locations that are treated in the same manner as any other read/write memory.

The MPU also provides a timing signal to PIA via the Enable input. The Enable (E) pulse is used to condition the PIA's internal interrupt control circuitry and for the timing of the peripheral control signals. Since all data transfers take place during the  $\phi_2$  portion of the clock cycle, the Enable pulse is normally  $\phi_2$ .

The 'peripheral side' of the PIA includes two 8 bit-bidirectional data bus (PA0-PA7 and PBO-PB7) and four interrupt/control lines CA1, CA2, CB1 and CB2. All of these lines on the 'Peripheral side' of the PIA are compatible with Standard TTL logic.

An expanded Block Diagram of the PIA is shown in Fig. 6.4. Internally, the PIA is divided into two symmetrical independent register configurations. Each half has three main features : an output register, a control register and a Data Direction Register. It is these registers that the MPU treats as memory location i.e., they can be either read from or written into. The output and Data Direction Registers on each side represent a single memory location to the MPU. Selecting between them is internal to the PIA and is determined by a bit in their control register.

The Data Direction Registers (DDR) are used to establish each individual peripheral bus line as either an input or an output. This is accomplished by having MPU write 'ones' or 'zeros' into the eight bit position of the DDR. Zeros or ones cause the corresponding peripheral data lines to function as inputs or outputs, respectively.

The Output Registers, ORA and ORB, when addressed , store the data present on the MPU Data Bus during an MPU write operation. This data will also appear on those peripheral lines that have been programmed as outputs. If a peripheral lines has been programmed as an input, the corresponding bit position of the output register can still be written into by the MPU, however, the data will be influenced by the external signal applied on that peripheral data line.

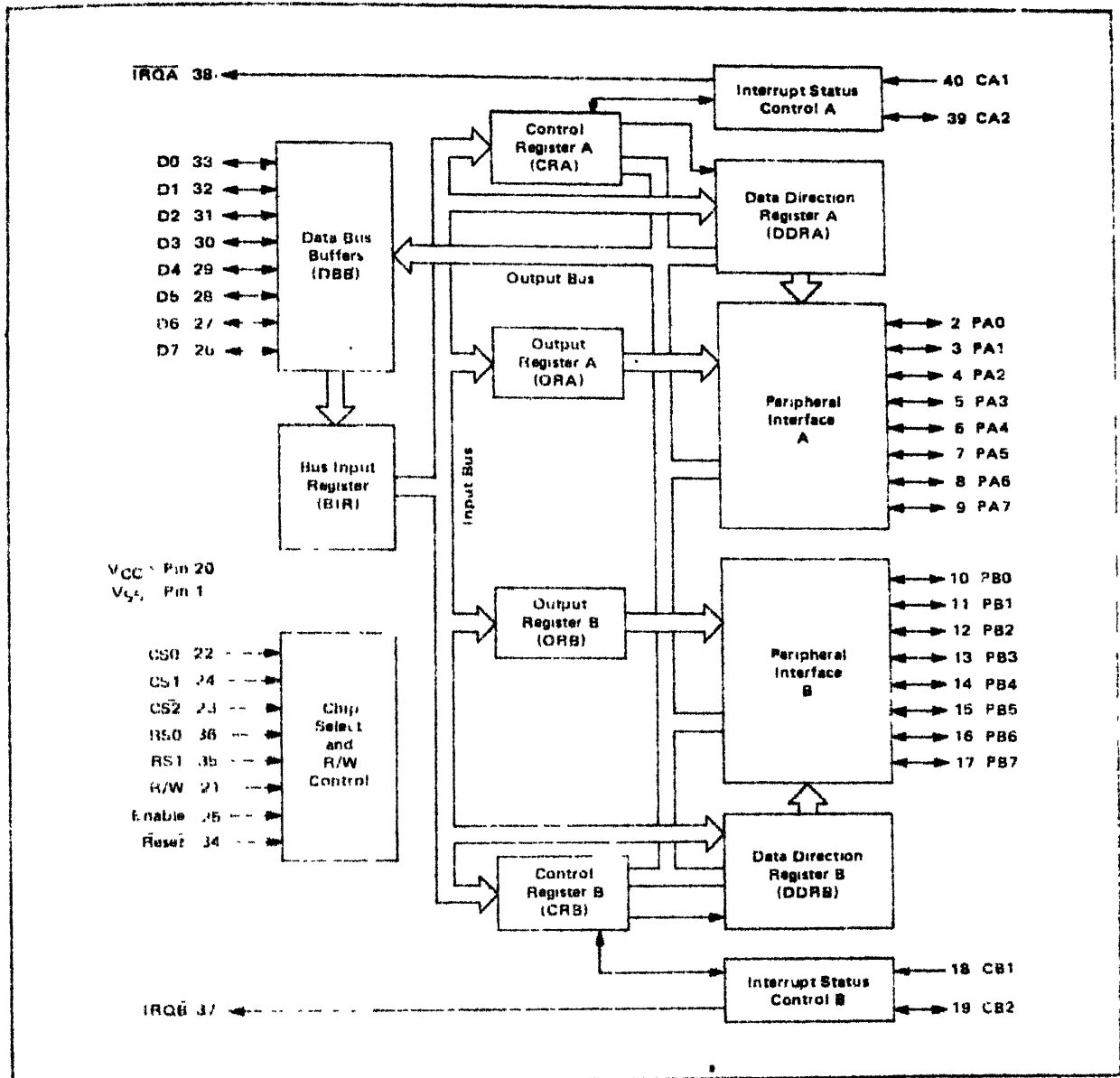


FIGURE 6-4 MC6820 PIA - Block Diagram

**Determine Active CA1 (CB1) Transition for Setting Interrupt Flag IRQA(B)1 – (bit b7)**

- b1 = 0 · IRQA(B)1 set by high-to-low transition on CA1 (CB1).  
 b1 = 1 · IRQA(B)1 set by low-to-high transition on CA1 (CB1).

**IRQA(B) 1 Interrupt Flag (bit b7)**

Goes high on active transition of CA1 (CB1). Automatically cleared by MPU Read of Output Register A(B). May also be cleared by hardware Reset.

**CA1 (CB1) Interrupt Request Enable/Disable**

- b0 = 0 Disables IRQA(B) MPU Interrupt by CA1 (CB1) active transition.<sup>1</sup>  
 b0 = 1 Enable IRQA(B) MPU Interrupt by CA1 (CB1) active transition.  
 1. IRQA(B) will occur on next (MPU generated) positive transition of b0 if CA1 (CB1) active transition occurred while interrupt was disabled.

b7	b6	b5	b4	b3	b2	b1	b0
IRQA(B)1 Flag	IRQA(B)2 Flag	CA2(CB2) Control			DDR Access	CA1(CB1) Control	

**IRQA(B)2 Interrupt Flag (bit b6)**

CA2 (CB2) Established as Input (b5 = 0) Goes high on active transition of CA2 (CB2). Automatically cleared by MPU Read of Output Register A(B). May also be cleared by hardware Reset.

CA2 (CB2) Established as Output (b5 = 1) IRQA(B)2 = 0, not affected by CA2 (CB2) transitions.

**Determines Whether Data Direction Register Or Output Register is Addressed**

- b2 = 0 · Data Direction Register selected.  
 b2 = 1 Output Register selected.

**CA2 (CB2) Established as Output by b5 = 1**

b5	b4	b3	(Note that operation of CA2 and CB2 output functions are not identical)
1	0	→ CA2	
		b3 = 0	<b>Read Strobe With CA1 Restore</b> CA2 goes low on first high-to-low F transition following an MPU Read of Output Register A, returned high by next active CA1 transition.
		b3 = 1	<b>Read Strobe with E Restore</b> CA2 goes low on first high-to-low E transition following an MPU Read of Output Register A, returned high by next high-to-low E transition.
		→ CB2	
		b3 = 0	<b>Write Strobe With CB1 Restore</b> CB2 goes on low on first low-to-high E transition following an MPU Write into Output Register B, returned high by the next active CB1 transition.
		b3 = 1	<b>Write Strobe With E Restore</b> CB2 goes low on first low-to-high E transition following an MPU Write into Output Register B, returned high by the next low to high E transition.

b5	b4	b3	
1	1	→ Set/Reset CA2 (CB2)	
			CA2 (CB2) goes low as MPU writes b3 = 0 into Control Register. CA2 (CB2) goes high as MPU writes b3 = 1 into Control Register.

**CA2 (CB2) Established as Input by b5 = 0**

b5	b4	b3	
0		→ CA2 (CB2) Interrupt Request Enable/Disable	
		b3 = 0	Disables IRQA(B) MPU Interrupt by CA2 (CB2) active transition. <sup>1</sup>
		b3 = 1	Enables IRQA(B) MPU Interrupt by CA2 (CB2) active transition.  1. IRQA(B) will occur on next (MPU generated) positive transition of b3 if CA2 (CB2) active transition occurred while interrupt was disabled
		→ Determines Active CA2 (CB2) Transition for Setting Interrupt Flag IRQA(B)2 – (bit b6)	
		b4 = 0	IRQA(B)2 set by high-to-low transition on CA2 (CB2).
		b4 = 1	IRQA(B)2 set by low-to-high transition on CA2 (CB2).

FIGURE 6-5 PIA Control Register Format

During an MPU Read operation, the data present on peripheral lines programmed as inputs is transferred directly to the system Data Bus. Due to differing circuitry, the results of reading positions programmed as outputs differ slightly between sides A and B of the PIA. On the B side, there is three-state buffering between Output Register B and peripheral lines such that the MPU will read the current contents of ORB for those bit positions programmed as outputs. During an MPU Read of the A side, the data present on the peripheral lines will affect the MPU Data regardless of whether the lines are programmed as outputs or inputs. The bit positions in ORA designated as outputs will be read correctly only if the external loading on the peripheral lines is within the specifications for one TTL load. That is, logic one used could be read as a logic zero if excessive loading reduced the voltage below 2.0 Volts.

The two control registers, CRA and CRB, allow the MPU to establish and control the operating modes of the peripheral control lines CA1, CA2, CB1 and CB2. It is by means of these four lines that control information is passed back and forth between the MPU and peripheral devices. The control word format and a summary of its features is shown in Fig. 6.5.

The following are the input signals available for processing :

1. Eight processed signals from the axle counter transducers.



2. One signal from the lock indicator output to be given to one of the interrupts pins of the PIA.
3. One signal from the hotbox detector output to be given to another interrupt pin of the PIA.
4. Another input which is produced by the logic, from the eight axle counter transducer signals for producing interrupts
5. A signal by whose status the processor would be able to decide upon the information about the track configuration at which transducers are installed.

The outputs to be provided from the PIA are :

1. to energize CLEAR relay to give CLEAR indication at the track side
2. to energize ENGAGED relay to give ENGAGED indication at the track side
3. to energize FAULT relay to give FAULT indication.

Therefore, it is necessary that three of the four interrupt pins of the PIA have to be enabled to produce an interrupt to the MPU. Although interrupt pins can be programmed to be active for any transition (high to low or low to high), they are programmed for high to low transition to be active. That is whenever a high to low transition is recognised on these pins an interrupt is generated by the PIA to the MPU. Eight pins of the peripheral side A of the PIA are programmed as inputs and are given processed signals

of the axle counter transducers. Pin PB7 of the peripheral side B is programmed as input whose status gives an information about the track configuration to the processor. All other pins of the peripheral side B of the PIA are programmed as outputs out of which PBO gives ENGAGED indication, PB1 gives CLEAR indication and PB2 gives FAULT indication. That is whenever CLEAR indication is to be given PB1 is made logical 0 and PB2 is made logical 1 by the MPU. Similarly, PBO for the ENGAGED signal, PB1 for the CLEAR signal and PB2 for the FAULT signal are made logical 1. The algorithm for initialization is given below.

Initialization algorithm :

1. Select the control registers of A side and B side (select PIACRA, PIACRB)
2. Select the Data Direction registers of sides A and B side (PIADRA, PIADRB) by writing the bit of PIACRA, PIACRB as zero (Fig. 6.5)
3. Make the PA0 through PA7 pins as inputs by writing all bits of PIADRA as 'zeros'.
4. Make PBO through PB6 as outputs and PB7 as input by writing all bits of PIADRB as 'ones' except eighth bit.
5. Select PIACRA and PIACRB.
6. Select both the output registers and make the interrupt pins to be active for high to low transition by writing the bits of PIACRA, PIACRB accordingly.

The actual program can be seen from the initialization routine in the program listing given at the end of the thesis.

## 6.2 CLEARING THE COUNTS AND BUFFERS

After the initialization is over the program has to clear the screen, and the buffers and counters maintained. In random access memory (RAM) these counters and buffers are maintained. These counters and buffers are maintained in consecutive locations in the RAM so that a small loop of about 5 lines of program can clear them. In the RAM two types of counters are maintained. One is four sets of local counters and the other is global counters. Each set of the local counters contains local IN1, local IN2, local OUT1, local OUT2 in it and these are incremented only when the MPU decides that the count generated is due to its corresponding transducer pair. Global counters also contains global IN1, global IN2, global OUT1 and global OUT2 in it and are incremented correspondingly whenever any of the corresponding local count is incremented. That is whenever any of the local IN1 is incremented global IN1 is incremented, whenever any of the local IN2 is incremented global IN2 is incremented and so on. In the program five buffers are maintained for storing the information of the counts to be displayed by the display routine. The buffers contain the following information.

1. The code for the graphics cursor position where the counts are to be displayed on the CRT screen.
2. IN and OUT counts to be displayed in binary form.
3. Code for the message to be sent to the terminal about the occupancy of the track section.

### 6.3 DISPLAYING THE TRACK CONFIGURATION

After clearing the screen, the buffers and the counters, the program checks the status of the pin PB7 of the PIA. If it is zero the pictorial representation of track configuration shown in Fig. 6.6a is displayed with the message 'TRACK IS CLEARED', otherwise the track configuration shown in Fig. 6.6b is displayed on the CRT terminal. After displaying the appropriate track configuration the processor stores the status of the track transducers outputs in a status byte maintained in the RAM and then waits for an interrupt.

When an interrupt is recognised processor checks the source of the interrupt by checking the 8th and the 7th bits of PIACRA and PIACRB. If the eighth bit of PIACRA is set then processor branches over to the axle counting routine. If the 7th bit of PIACRA is set it knows that the interrupt is due to lock indication failure and gives a fault indication. If the 8th bit of PIACRB is set then it jumps to the hotaxle routine.

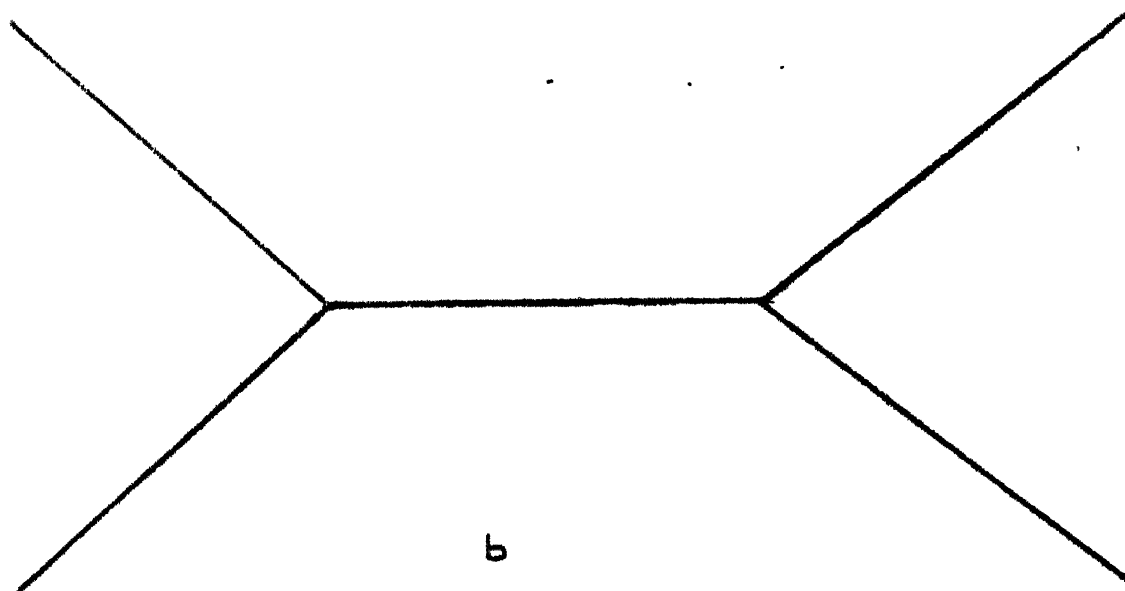
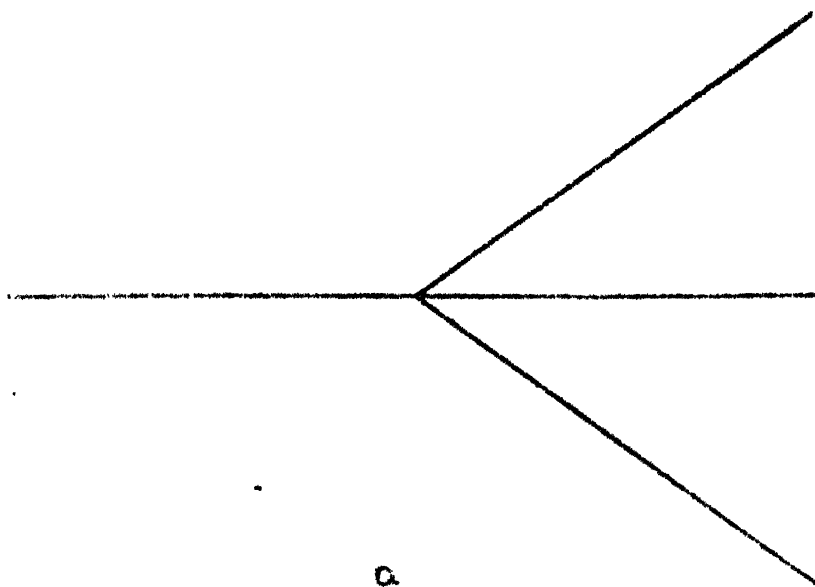


FIG 5.5. PICTORIAL REPRESENTATION OF  
THE TWO POSSIBLE TRACK-  
SECTIONS

#### 6.4 AXLE COUNTING ROUTINE

After recognising that the interrupt is generated due to the axle counting transducers, processor takes the present status of the track transducers and does 'exclusive-OR' with the previous status stored in the status byte to find the particular transducer that has changed its status due to the wheel of the train. At the same time it makes PBO 'logical1' to indicate that the track is ENGAGED. Then the particular bit of the status byte corresponding to the changed status is updated accordingly. Afterwards the processor checks for the status of the other transducer in the transducer pair and increments the corresponding Global count. Then it checks for the vacant buffer and fills the first byte of the buffer with the code corresponding to the graphic cursor position of the local count to be displayed. In the RAM one buffer flag corresponding to each buffer is maintained to indicate whether that buffer is full or vacant. A buffer flag is zero indicates the vacancy and new data can be entered, otherwise the buffer is full. Then it increments the corresponding local count and fills the consecutive bytes of the buffer with the binary value of the local count to be displayed. Finally, last byte of the buffer is filled with the code corresponding to the message to be displayed on the CRT terminal. Then the buffer flag is cleared. If this byte is zero the message 'TRACK IS ENGAGED' is displayed, otherwise 'TRACK IS CLEARED' is



displayed. If the track is cleared PB7 is made 'logical1' indicating that the track is clear which energises 'CLEAR RELAY'. Before incrementing outcount the processor checks that the corresponding incout is zero or not. If it is zero it gives fault signal because without an incout, outcount cannot be registered. This shows some extraneous signal or some malfunctioning of the processor or peripherals.

After incrementing the appropriate count and filling the corresponding buffers the processor goes to the display routine and it starts displaying the counts and the message about the track status. After it completes displaying one buffer it clears the buffer flag indicating that new data can be loaded into it. In this processes of display if any interrupt is recognised the processor stops the display at that point storing the information about its status and attends to its interrupt routine and comes back to its original status and starts doing it. If again an interrupt is recognised similar action takes place. If all buffers are displayed and still interrupt is not recognised then processor waits for an interrupt. In displaying the count it changes the binary count stored to decimal count and displays. Shunting movement of a train can be interpreted if both IN count and OUT count are displayed at the same transducer. This count does not correspond to the exact number of wheels entered or left the track because one wheel can produce all



the count, whereas in through running this corresponds to the exact number of wheels that have entered and left.

#### 6.5 HOTBOX DETECTION ROUTINE

After recognising that the interrupt is due to the output from the hotbox detector, processor comes to this routine.

When first incount is registered in axle counting routine, processor checks whether this incount is generated by the axle counting transducer kept by the side of the hotbox detector. If not, 'Hotbit', which is maintained in the RAM is cleared. This hotaxle detection routine first checks whether 'hotbit' is zero or not. If it is zero it assumes that hotaxle is produced when train is entering the track and it takes incount for displaying the number of wheel. Otherwise outcount is taken for displaying the exact number of wheel which is hot. Details can be seen from the programme listings given at the end of the thesis.

## CHAPTER 7

## CONCLUSIONS

The software is developed for a combined system of axle-counting and hotbox detection, assuming that the processed signals are available from the respective transducers.

The software has the following features :

1. It takes care of four detection point axle-counting system and can easily be modified for more detection points.
2. It has the maximum counting capacity of  $2^{15}$  wheels, which can be extended further.
3. It provides a visual information of the status of the track-section of interest.
4. In the fail safety point of view, although it can not pinpoint the particular component in the system that is mal-functioning, it provides a 'FAULT' indication along with the 'ENGAGED' signal whenever there is a lock-failure or some other failure producing logically in-compatible count.

The system has been tried out successfully by simulating real time signals using a toy train system. However, a more thorough testing of the performance of the system in an actual environment is required.

The following features can be incorporated for the further improvement of the present system.

1. To facilitate a convenient visual display for the status of the track, it is suggested that the track section that is engaged is displayed differently, for example by a dotted line, compared to the section that is clear. At the approaching point for the engaged track section only the incount need be displayed and at the outgoing point the outcount.
2. After the completion of the display function, the processor can be used for self-check of the system, before an interrupt is recognised. This ensures improved fail-safety and better utilization of the microprocessor capabilities.
3. Instead of making the decision about the occurrence of the hotbox on a pre-set threshold, it is preferable to record the output of the hotbox detector corresponding to the each of the bearings and suitably process them. A decision based on such a scheme will result in lesser false alarms, [9] because in this case the threshold will be set according to the actual average conditions of the bearings of the particular train, rather than a global minimum threshold set apriori.

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9. 'A User's guide to the silicon chip Microprocessors', Railway Gazette International, November 1981, vol. 137, No.11, pp. 943-957.

10. 'M6800 Microprocessor Application Manual', Motorola Semiconductor Products Inc., 1975.
11. 'M6800 Microprocessor Programming Manual', Motorola Semiconductor Products Inc., 1975.

## APPENDIX

The simulated signals are generated using photodetectors and light sources. When train passes over the light source the required transition is produced.

The circuit diagram used for interrupt generation is given in Fig. A-1. Only two detection point axle counting system is simulated because of the nonavailability of cross-overs. The signals from the transducers are given to one port of 4-bit magnitude comparator (7485). The same signals are given to D-flip flops, whose outputs are given to the other port of the comparator. 'A=B' output is given to a monoshot and clock pin of D-flip flops through AND gate whose other input is output of a oscillator. The details can easily be understood from the circuit diagram.

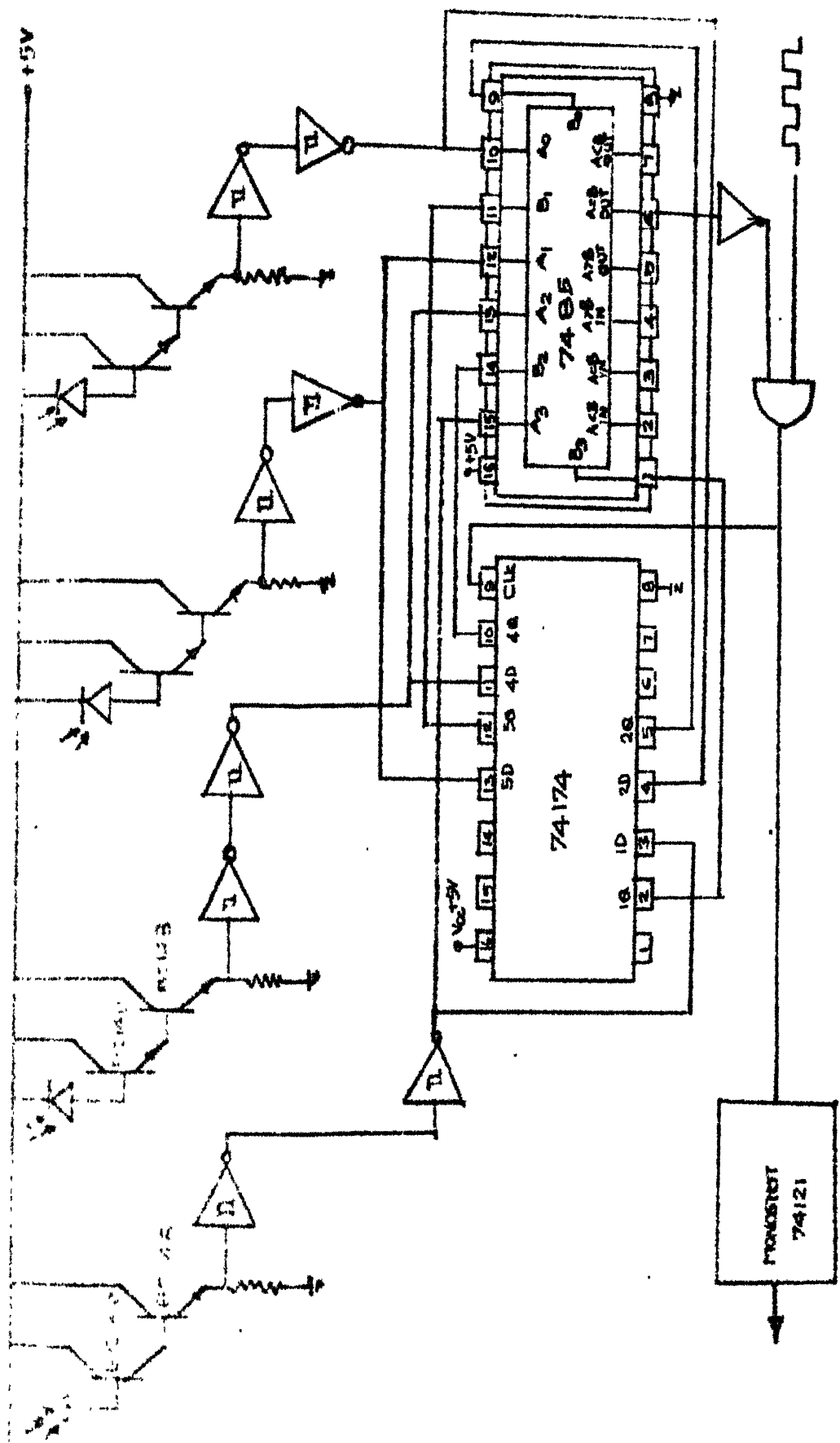


FIG. 1. INTERRUPT GENERATION CIRCUIT

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A S S F M P L Y - L I S T I N G

\*\*\*\*\*



FPCF	ACIACF	EQU	\$FPCF
FPCF	ACIASF	EQU	\$FPCF
FPCF	ACIADF	EQU	\$FPCF
0030	STQPEA	EQU	\$0030
FPC9	FIACFA	EQU	\$FPC9
FPC8	FIACFA	EQU	\$FPC8
FPC8	FIADFA	EQU	\$FPC8
FPCA	FIACFP	EQU	\$FPCA
FPCA	FIADFP	EQU	\$FPCA
FPCF	FIACFP	EQU	\$FPCF
0000	STPYT	EQU	\$0000
0001	CNT1	EQU	\$0001
0002	CNT2	EQU	\$0002
0003	IN11	EQU	\$0003
0004	IN1	EQU	\$0004
0005	IN22	EQU	\$0005
0006	IN2	EQU	\$0006
0007	OUT11	EQU	\$0007
0008	OUT1	EQU	\$0008
0009	OUT22	EQU	\$0009
0004	OUT2	LOC	\$0004
002F	CHPYT1	EQU	\$002F
002C	CHPYT2	EQU	\$002C
002I	CHPYT3	EQU	\$002I
002E	CHPYT4	EQU	\$002E
002F	HTP1T	EQU	\$002F
0003	CLPIND	EQU	\$0003
002A	CLPE11	EQU	\$002A
E009	INDEX	EQU	\$E009
E000	INDEX1	EQU	\$E000
0031	INDEX2	EQU	\$0031
0033	SAVEP	EQU	\$0033
0034	SAVEX1	EQU	\$0034
0036	PFLIND	EQU	\$0036
0040	PUF1PT	EQU	\$0040
0041	PUF2PT	EQU	\$0041
0042	PUF3PT	EQU	\$0042
0043	PUF4PT	EQU	\$0043
0044	PUF5PT	EQU	\$0044
0045	PUFIND	EQU	\$0045
0064	PUFEND	EQU	\$0064
0047	ISTPUF	EQU	\$0047
0041	SNIPUF	EQU	\$0041
0053	THDPUF	EQU	\$0053
0059	FPTEUF	EQU	\$0059
005F	FFHEUF	EQU	\$005F
FFF8	INTVCT	EQU	\$FFF8
E000		ORG	\$E000
E000		PME	1
E001 80 40 20		FCF	\$80, \$40, \$20, \$10, \$08, \$04, \$02, \$01
E009		PME	2
E00F 00 0F 00		FOE	\$00, \$0E, \$00, \$13, \$00, \$1E, \$00, \$23
E013 0D 0A FF NEG1		FCF	\$0D, \$0A, \$FF

E041	01 03	HTIT	FCP	\$01,\$03
E042	1P 2A	**	FIGURE1	-- GRAPHICS DATA FOR FIGURE ONE
E04F	20 61 32	FIGURE1	FCB	\$1P,\$2A
0,507		FCC		*PA250,150 550,150A450,150 550,250A8
E076	1P 2A	FCP		\$1P,\$2A
E078	64 6P 32	FCC		*TK200,2000S
E083	1P 2A	FCP		\$1P,\$2A
E09F	6D 34 61	FCC		*M4A2MIN36PIN OUT
E096	1P 2A	FCB		\$1P,\$2A
E098	64 6P 3F	FCC		*DK500,3000SIN OUT
E0A4	1P 2A	FCB		\$1P,\$2A
E0AC	64 6P 3F	FCC		*DK500,2000SIN OUT
E0PF	1P 2A	FCB		\$1P,\$2A
E0CC	64 6P 3F	FCC		*DK500,500SIN OUT
E0I1	1P 2A	FCB		\$1P,\$2A
E0I3	6D 34 61	FCC		*M4A1MIN36P
E0DI	1P 2A	FCB		\$1P,\$2A
E0DF	64 54	FCC		*LT
E0E1	FF	FCB		\$FF
E0E2	1P 2A	**	FIGURE2	-- GRAPHICS DATA FOR FIGURE TWO
E0E4	20 61 31	FIGURE2	FCB	\$1P,\$2A
E10T	22 3F 20	FCC		*PA150,250 250,150 450,150 550,250A8
E124	1P 2A	FCC		*250,150A450,150 550,502
E126	64 6P 31	FCB		\$1P,\$2A
E131	1P 2A	FCC		*TK100,2000S
E132	6D 34 61	FCB		\$1P,\$2A
E144	1P 2A	FCC		*M4A2MIN36PIN OUT
E146	64 6P 3F	FCB		\$1P,\$2A
E153	1P 2A	FCC		*DK500,3000SIN OUT
E15A	64 6P 31	FCB		\$1P,\$2A
E16P	1P 2A	FCC		*DK100,500SIN OUT
E16T	64 6P 3F	FCB		\$1P,\$2A
E17F	1P 2A	FCC		*DK500,500SIN OUT
E180	6D 34 61	FCB		\$1P,\$2A
E18A	1P 2A	FCC		*M4A1MIN36P
E18C	64 54	FCB		\$1P,\$2A
E18F	FF	FCC		*LT
E18F	1P 2A	FCB		\$FF
E191	64 6P 32	**	CUPS11	-- FIRST POSITION OF THE CURSOR
E19C	FF	*		OF THE FIRST FIGURE.
E19D	1P 2A	CUPS11	FCB	\$1P,\$2A
E19F	64 6P 3F	FCC		*TK200,1800S
E1AA	FF	FCB		\$FF
E1AP	1P 2A	**	CUPS12	-- SECOND POSITION OF THE CURSOR
E1AT	64 6P 3F	*		OF THE FIRST FIGURE.
E1B8	FF	CUPS12	FCB	\$1P,\$2A
E1B9	1P 2A	FCC		*DK500,1800S
E1BP	64 6P 3F	FCB		\$FF
E1CE	FF	**	CUPS13	-- THIRD POSITION OF THE CURSOR.
E1D9	1P 2A	CUPS13	FCB	\$1P,\$2A
E1DP	64 6P 3F	FCC		*DK500,2800S
E1E5	FF	FCB		\$FF
E1F9	1P 2A	**	CUPS14	-- FOURTH POSITION OF THE CURSOR.
E1FP	64 6P 3F	CUPS14	FCB	\$1P,\$2A
E1CF	FF	FCC		*DK500,300S
		FCB		\$FF

```

**      CUP521 -- FIRST POSITION OF THE CUP50F
*      OF THE SECOND FIGURE.
F1C6  1P 2A      CUP521 FCP      $1P,$2A
F1C8  64 6P 31   FCC      'TK100,2807S'
F1D3  FF          FCP      $FF
**      CUP522 -- SECOND POSITION OF THE CUP50F
*      OF THE SECOND FIGURE.
F1D4  1P 2A      CUP522 FCP      $1P,$2A
F1D6  64 6P 31   FCC      'TK100,307S'
E1E0  FF          FCP      $FF
F1F1  20 20 20   PLANK  FCC      '
E1F5  FF          FCP      $FF
**      CLFOP1 -- DATA STORED FOR CLEARING THE
*      COUNT DISPLAYED ON FIGURE ONE.
F1F6  1P 2A      CLFOP1 FCP      $1P,$2A
E1F8  64 6P 32   FCC      'TK200,1807S'
F202  1P 2A      FCP      $1P,$2A
F204  64 6P 35   FCC      'TK500,2807S'
F21F  1P 2A      FCP      $1P,$2A
E220  64 6P 35   FCC      'DK500,307S'
E23A  1P 2A      FCP      $1P,$2A
E23C  64 6P 35   FCC      'DK500,1807S'
E2F6  1P 2A      FCP      $1P,$2A
E2F8  64 54      FCC      'DT'
E2FA  FF          FCP      $FF
**      CLFOP2 -- DATA STORED FOR CLEARING THE
*      COUNT DISPLAYED ON FIGURE-TWO.
E2FP  1P 2A      CLFOP2 FCP      $1P,$2A
E2FD  64 6P 31   FCC      'TK100,2807S'
E277  1P 2A      FCP      $1P,$2A
E279  64 6P 35   FCC      'DK500,2807S'
E293  1P 2A      FCP      $1P,$2A
E295  64 6P 35   FCC      'DK500,307S'
F2AF  1P 2A      FCP      $1P,$2A
E2F1  64 6P 31   FCC      'DK100,307S'
F2CF  1P 2A      FCP      $1P,$2A
E2CT  64 54      FCC      'IT'
E2CF  FF          FCP      $FF
**      CLFPHYT -- 'CLEAR BYTE'
*      -- USED FOR CHECKING THE EMPTINESS
*      -- OF THE TPACK SECTION.
E2D0  FF          CLFPHYT FCP      $FF
**      CLEARP -- 'CLEARED'
*      -- USED FOR SENDING THE MESSAGE
*      -- 'TPACK IS CLEARED'.
F2D1  1P 2A      CLEARP FCP      $1P,$2A
E2D3  6D 34 61   FCC      'M4A2MIN3CP'
E2TT  1P 2A      FCP      $1P,$2A
E2TF  64 6P 31   FCC      'TK10,3500STRACK IS CLEARED'
F2F9  1P 2A      FCP      $1P,$2A
E2FE  6D 34 61   FCC      'M4A1MIN3CP'
F305  1P 2A      FCP      $1P,$2A
E307  64 54      FCC      'DT'
E309  FF          FCP      $FF

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E30A	1P 2A	ENGAGE	FCC	-- 'TRACK IS ENGAGED'	
E30C	6D 2A 61		FCC	\$1P,\$2A	
E316	1P 2A		FCC	'M4A2M1N3CF'	
E318	6A 6P 21		FCC	\$1P,\$2A	
E332	1P 2A		FCC	'TK10,3500STEACK IS ENGAGED'	
E334	6D 2A 61		FCC	\$1P,\$2A	
E33F	1P 2A		FCC	'M4A1M1N3CF'	
E340	6A 5A		FCC	\$1P,\$2A	
E342	FF		FCC	'DT'	
			FCC	\$FF	
		**	SCFCLF	-- 'SCFFEN CLEAR'	
		*		-- USED FOR CLEARING THE	
		*		-- GRAPHICS DISPLAY ON THE CPT.	
E343	1P 2A	SCFCLF	FCC	\$1P,\$2A	
E345	6A 41		FCC	'DA'	
E347	FF		FCC	\$FF	
		**	PUFFLT	-- 'BUFFER FAULT'	
		*		-- USED TO INDICATE BUFFER	
		*		-- OVERFLOW.	
E348	42 5F 46	PUFFLT	FCC	'BUFFER OVERFLOW'	
E357	FF		FCC	\$FF	
		**	INITPT	-- INITIALIZATION ROUTINE	
E358	86 00	INITPT	LDA A	#300	
E35A	P7 FP C9		STA A	PIACPA	
E35D	P7 FP CP		STA A	PIACPE	
E360	C6 7F		LDA P	#37F	
E362	P7 FP C8		STA A	PIADPA	
E365	F7 FP CA		STA P	PIADPE	
E368	86 0D		LDA A	#30D	
E36A	P7 FP C9		STA A	PIACPA	
E36D	P7 FP CP		STA A	PIACPE	
E370	CF E3 43		LIX	#SCFCLF	CLEAR THE SCREEN
E373	PD E7 CD		JSP	OUTSTF	
E376	P6 FP CA		LDA A	PIADPE	
E379	8F 90		PIT A	#380	
E37F	27 05		PEQ	FIG1	
E37D	CF E0 E2		LIX	#FIGFE2	
E380	PD E7 CD		JSP	OUTSTF	
E383	20 06		RPA	STAPT1	
E385	CE E0 43	FIG1	LIX	#FIGFE1	
E388	PD F7 CD		JSP	OUTSTF	
E38F	P6 FP C8	STAPT1	LDA A	PIADPA	
E38E	97 00		ST4	STIYT	
E390	86 01		LDA A	#301	
E392	97 2F		STA A	HTFIT	
E394	PD E7 CP		JSP	CLRFT	
E397	CE E2 D1		LIX	#CLEAPI	
E39A	PD F7 CD		JSP	OUTSTF	
E39D	CE E6 11		LIX	#INTPT	
E3A0	FF FF F8		STX	INTVCT	
E3A2	0F		CLI		
		**	DISPLAY ROUTINE		
		**	ISTPFT	-- 1ST BUFFER-FLAG TEST	
		*		-- TESTS EMPTYNESS OF	
		*		-- THE FIRST BUFFER	
E3A4	7D 00 40	ISTPFT	TST	BUFIPT	

E3A7	26 24		PNE	ISPFFL
		**	SNIPFT	-- '2ND BUFFER-FLAG TEST'
		*		-- TEST THE EMPTINESS OF
		*		-- THE SECOND BUFFER
E3A9	7D 00 41	SNIPFT	TST	PUF2PT
E3AC	26 2C		PNE	SDPFFL
		**	THIPFT	-- '3RD BUFFER-FLAG TEST'
		*		-- TESTS THE EMPTINESS OF
		*		-- THE THIRD BUFFER
E3AF	7D 00 42	THIPFT	TST	PUF3PT
E3B1	26 34		PNE	TDPFFL
		**	FTHPFT	-- '4TH BUFFER-FLAG TEST'
		*		-- TESTS THE EMPTINESS OF
		*		-- THE FOURTH BUFFER
E3B3	7D 00 43	FTHPFT	TST	PUF4PT
E3B6	26 3C		PNE	FDPFFL
		**	FFHPFT	-- '5TH BUFFER-FLAG TEST'
		*		-- TESTS THE EMPTINESS OF
		*		-- THE FIFTH BUFFER
E3B8	7D 00 44	FFHPFT	TST	PUF5PT
E3BP	26 FF		PNE	FFHPFT
E3BD	3F		WAI	
E3BE	2C E4		BPA	ISTPUF
		**	FFHPFL	-- '5TH BUFFER FULL'
E3C0	CF 00 5F	FFHPFL	LIX	#FFHBUF
E3C3	DF 36		STX	BFLIND
E3C5	PD E4 01		JSP	BFDSP
E3C8	7F 00 44		CLR	PUF5PT
E3CB	20 F7		BPA	ISTPFT
		**	ISPFFL	-- '1ST BUFFER FULL'
E3CD	CF 00 47	ISPFFL	LIX	#ISTPUF
E3D0	DF 36		STX	BFLIND
E3D2	PD E4 01		JSP	BFDSP
E3D5	7F 00 40		CLR	PUF1PT
E3D8	20 CF		BPA	SNIPFT
		**	SDPFFL	-- '2ND BUFFER FULL'
E3DA	CF 00 4D	SDPFFL	LIX	#SNIPUF
E3DD	DF 36		STX	BFLIND
E3DF	PD E4 01		JSP	BFDSP
E3E2	7F 00 41		CLR	PUF2PT
E3E5	20 C7		BPA	THIPFT
		**	TDPFFL	-- '3RD BUFFER FULL'
E3E7	CF 00 53	TDPFFL	LIX	#THDEUF
E3EA	DF 36		STX	BFLIND
E3EC	PD E4 01		JSP	BFDSP
E3EF	7F 00 42		CLR	PUF3PT
E3F2	20 BF		BPA	FTHPFT
		**	FDPFFL	-- '4TH BUFFER FULL'
E3F4	CF 00 59	FDPFFL	LIX	#FDPBUF
E3F7	DF 36		STX	BFLIND
E3F9	PD E4 01		JSP	BFDSP
E3FC	7F 00 43		CLR	PUF4PT
E3FF	20 P7		BPA	FFHPFT
		**	PFDSP	-- 'BUFFER DISPLAY ROUTINE'
		*		-- DISPLAYS THE CONTENTS OF

E403	81	01	CMF A	#301
E405	27	1A	PEQ	FFFTPN
E407	81	02	CMF A	#302
E409	27	20	HEQ	FFSTPN
E40P	81	03	CMF A	#303
E40T	27	26	PEQ	THITPN
E40F	81	04	CMF A	#304
E411	27	2C	PEQ	FPTTPN
E413	81	05	CMF A	#305
E415	27	32	PEQ	FFFTPN
E417	CE	F1 1A	LIX	#CUPS22
E41A	PD	F7 CI	JSP	OUTSTP
E41T	PI	F4 F3	JSP	DSPLAY
E420	39		PTS	
** FFFTPN -- '1ST FIGURE FIRST TRANSDUCER'				
E421	CE	F1 8F	FFFTPN LIX	#CUPS11
E424	PD	F7 CI	JSP	OUTSTP
E427	PI	F4 F3	JSP	DSPLAY
E42A	39		PTS	
** FFSTPN -- '1ST FIGURE SECOND TRANSDUCER'				
E42P	CE	F1 9D	FFSTPN LIX	#CUPS12
E42E	PD	F7 CI	JSP	OUTSTP
E431	PD	F4 F3	JSP	DSPLAY
E434	39		PTS	
** THITPN -- 'THIPI TRANSDUCER'				
E43F	CE	F1 AP	THITPN LIX	#CUPS13
E43S	PD	F7 CI	JSP	OUTSTP
E43P	PD	F4 F3	JSP	DSPLAY
E43F	39		PTS	
** FPTTPN -- '4TH TRANSDUCER'				
E43F	CE	F1 PD	FPTTPN LIX	#CUPS14
E442	PD	F7 CI	JSP	OUTSTP
E445	PD	F4 F3	JSP	DSPLAY
E448	39		PTS	
** SFFTPN -- '2ND FIGURE FIRST TRANSDUCER'				
E449	CE	F1 C6	SFFTPN LIX	#CUPS21
E44C	PD	F7 CI	JSP	OUTSTP
E44F	PD	F4 F3	JSP	DSPLAY
E452	39		PTS	
** DSPLAY -- 'DISPLAY'				
* -- DISPLAYS THE CONTENTS				
* -- THE PUFFER CHOSEN				
E453	DE	36	DSPLAY LIX	PFLINI
E455	A6	01	LIA A	1.X
E457	E6	02	LIA B	2.X
E459	46		POF A	
E45A	F6		POF B	
E45P	PD	F6 43	JSP	CVPTD
E45F	CE	F1 F1	LIX	#PLANK
E461	PD	F7 CI	JSP	OUTSTP
E464	DE	36	LIX	PFLINI
E466	A6	03	LDA A	3.X
E468	E6	04	LDA B	4.X
E46A	46		POF A	
E46P	F6		POF B	

F46C	PI	F6	43		JSE	CVPTT
F46F	IF	36			LIX	EFFIND
F471	A6	05			LDA A	5,X
F473	AI				TST A	
F474	26	07			PNE	LCLFFT
F476	CF	E3	CA		LIX	#ENGAGE
F479	PI	E7	CI		JSE	OUTSTF
F47C	39				PTS	
F47D	F6	FF	CA	LCLFFT	LIA A	PIA7FE
F480	45	30			PIT A	#380
F482	27	08			PEC	LCLFT1
F484	CF	E2	5P		LIX	#CLF7F2
F487	PI	E7	CI		JSE	OUTSTF
F48A	11	06			PFA	CLEAR
F48C	CF	E1	FC	LCLFT1	LIX	#CLF7F1
F48F	PI	E7	CD		JSE	OUTSTF
F492	CF	E2	FI	CI FAP	LIX	#CLEARF
F495	PI	E7	CI		JSE	OUTSTF
F498	PI	E7	CI		JSE	CLFFT
F49F	39				PTS	
F49C	F6	FF	CB	STAPT	LIA A	PIA7FA
F49F	28	00			P7F A	STPYT
F4A1	CF	E0	00		LIX	#INIEX1
F4A4	00	01		TIPT	LIA F	#301
F4A6	F7	FF	CA		STA F	PIA7FF
F4A9	06	08			LIA F	#308
F4AB	D7	01			STA F	CNT1
F4AI	0C			L77F2	CLC	
F4AF	46				P7P A	
F4AF	97	30			STA A	STOFEA
F4P1	25	46			PCS	SUPPT1
F4P3	7A	00	01	L77P3	DEC	CNT1
F4P6	7D	00	01		TST	CNT1
F4P9	26	F2			PNE	L77P2
F4PP	F6	FF	CB		LDA A	PIA7PA
F4PF	F1	E2	DO		CMP A	CLPEYT
F4C1	26	2C			PNE	ENGRT
F4C3	26	04			LIA A	IN1
F4C5	21	08			CMP A	OUT1
F4C7	26	26			PNE	ENGFT
F4C9	26	03			LDA A	IN11
F4CP	21	07			CMP A	OUT11
F4CI	26	20			PNE	ENGRT
F4CF	26	06			LDA A	IN2
F4D1	21	0A			CMP A	OUT2
F4D3	26	1A			PNE	ENGFT
F4D5	26	05			LDA A	IN22
F4D7	21	09			CMP A	OUT22
F4D9	26	14			PNE	ENGFT
F4DP	86	02			LDA A	#302
F4DD	F7	FF	CA		STA A	PIAORB
F4E0	DE	45			LIX	BUFIND
F4E2	C6	01			LDA F	#301
F4E4	F7	05			STA F	5,X
F4E6	3P				RTI	

F4F0 F7 F6 CA  
F4F0 7E F6 02

ENGFT -- 'ENGAGED ROUTINE'  
\* -- GIVES THE INDICATION

F4EF 86 01  
F4F1 F7 F6 CA  
F4F4 DF 4F  
F4F6 6F 0F  
F4F8 3F  
F4F9 16 01  
F4FF 01 02  
F4FD 2E 0F  
F4FF 16 01  
F501 17 02  
F503 0F 02  
F505 17 01  
F507 1F F5 AF  
F50A 06 20  
F50C 20 4F  
F50E 16 01  
F510 00 02  
F512 17 02  
F514 8F 02  
F516 06 20  
F518 20 22  
F51A 8F 5F  
F51C 16 00  
F51E F5 00  
F520 27 11

ENGFT LDA A #301  
STA A FIAOFF  
LDX PUFIND  
CLP 5,X  
FTI  
SUPFT1 LDA F CNT1  
CMP F #304  
PCT SUPFT2  
SUPFT2 LIA F CNT1  
STA F CNT2  
ADD F #304  
STA F CNT1  
JSP PTCNT2  
LIA A STOREA  
RPA LOOP3  
SUPFT2 LDA F CNT1  
SUP F #304  
STA F CNT2  
RSP PTCNT1  
LIA A STOREA  
RPA LOOP3  
PTCNT1 RSP CHXFT1  
LIA F STEYT  
FIT F 0,X  
RPG LHTFT1

\*\* HLTF1 -- 'HIGH TO LOW TRANSITION ONE'

F522 F6 00  
F524 F3  
F525 14 00  
F527 17 00  
F529 8F 5A  
F52B 16 00  
F52D F5 00  
F52F 27 42  
F531 20 12

HLTF1 LIA F 0,X  
COM F UPDATING THE STATUSBYTE  
AND F STEYT  
STA F STEYT  
RSP CHXFT2  
LIA F STEYT  
FIT F 0,X  
RPG OUTICT OUTICOUNT  
RPA INICNT INICOUNT

\*\* LHTFT1 -- 'LOW TO HIGH TRANSITION ONE'

F533 16 00  
F535 1A 00  
F537 17 00  
F539 8F 4A  
F53B 16 00  
F53D F5 00  
F53F 26 52  
F541 20 02  
F543 20 42

LHTFT1 LIA F 0,X  
RPA F STEYT UPDATING THE STATUSBYTE  
STA F STEYT  
RSP CHXFT2  
LIA F STEYT  
FIT F 0,X  
RPG OUTICT  
RPA INICNT  
FLPT2 RPA FLPT

\*\* INICNT -- 'INICOUNT'

\* -- INCREMENTS THE GLOBAL AND  
\* -- LOCAL INICOUNTS

F545 16 02  
F547 F5

INICNT LDA F INI  
TST F



FF49	26	1F		PMF	MFCT1
FF4A	27			FSH F	
FF4F	0F	90		LDA F	#380
FF4D	FF	FF	CA	PIT F	PIAOPF
FF50	27	0F		PRG	ONEHD
FF52	01	F0	42	LIX	#HTIT-1
FF55	20	02		PPA	FILE
FF57	0F	F0	41	LIX	#HTIT
FF5A	16	00		FILE	02X
FF5C	FF	FF	08	PIT F	PIAOPF
FF5F	26	02		PMF	MFCT
FF61	2F	00	2F	CLF	HTPIT
FF64	32			FUL F	
FF65	50			INC F	
FF66	17	04		STA	INI
FF68	16	03		LDA F	INI1
FF6A	02	00		ALC F	#300
FF6C	17	03		STA F	INI1
FF6F	1D	F6	22	JSP	LCLCT1
FF71	1D	F6	4A	JSP	LINICT
FF72	22			PTS	
FF75	20	00		PPA	FLFT2
FF77	0F	F0	00	LIX	#INDEX1
FF7A	1F	2F		STX	CHPYT1
FF7C	16	20		LDA F	CHPYT2
FF7F	1F	01		ALL F	CNT1
FF80	17	20		STA F	CHPYT2
FF82	1E	2F		LIX	CHPYT1
FF84	32			PTS	
FF85	0F	F0	00	LIX	#INDEX1
FF88	1F	2F		STX	CHPYT3
FF8A	16	2E		LDA F	CHPYT4
FF8C	1F	02		ALL F	CNT2
FF8E	17	2F		STA F	CHPYT4
FF90	1E	2F		LIX	CHPYT3
FF92	32			PTS	
				OUTICT	-- 'OUTICOUNT'
					-- INCREMENTS GLOBAL ALL
					-- LOCAL OUTICOUNT
FF92	2D	00	04	OUTICT	INI
FF96	27	AF		PRG	FLFT2
FF98	16	08		LDA F	OUT1
FF9A	50			INC F	
FF9F	17	08		STA F	OUT1
FF9D	D6	07		LDA F	OUT11
FF9F	C9	00		ADC F	#300
FFA1	17	07		STA F	OUT11
FFA3	1D	E6	22	JSP	LCLCT1
FFA6	1D	E6	2C	JSP	LOUTIT
FFA9	1D	E6	F5	JSR	ORIGIN
FFAC	32			PTS	
FFAD	20	C6		PPA	FLRT4
FFAF	81	D4		PSP	CHXPT2
FFB1	D6	00		LDA F	STBYT

FFD0	50		COM P	UPDATING THE STATUSBYTE
FFFA	DA 00		AND P	STBYT
FFFC	17 00		STA P	STBYT
FFFE	4D 17		PSP	CHXFT1
FFC0	16 00		LIA P	STBYT
FFC2	FF 00		PIT P	0,X
FFC4	27 10		PER	IN2CNT
FFC6	20 22		RPA	OUT2CT
FFC8	16 00	LHFTPT2	LIA P	0,X
FFCA	DA 00		OPA P	STBYT
FFCC	17 00		STA P	STBYT
FFCE	8D A7		PSP	CHXFT1
FFD0	16 00		LIA P	STBYT
FFD2	15 00		PIT P	0,X
FFD4	27 15		PER	OUT2CT
		**	IN2CNT	-- 'IN1COUNT'
		*		-- INCREMENTS GLOBAL AND
		*		-- LOCAL IN1COUNTS
FFD6	DA 04		IN2CNT	LIA P
FFD8	FC		INC P	IN2
FFDA	17 06		STA P	IN2
FFDC	16 05		LIA P	IN22
FFDE	00 00		ATC P	#300
FFDF	17 05		STA P	IN22
FFE1	11 16 22		JSP	LCLCT1
FFE4	11 16 00		JSP	LIN2CT
FFE7	11 16 15		JSP	OPIGIN
FFFA	30		PTS	
		**	OUT2CT	-- 'OUT2COUNT'
		*		-- INCREMENTS GLOBAL AND
		*		-- LOCAL OUT2COUNTS
FFFB	71 00 04		OUT2CT	TST
FFFD	27 11		PER	FLPT3
FFFE	16 0A		LIA P	OUT2
FFFF	FC		INC P	
FFFF	D7 0A		STA P	OUT2
FFFF	16 02		LIA P	OUT22
FFFF	00 00		ATC P	#300
FFFF	D7 02		STA P	OUT22
FFFF	11 16 22		JSP	LCLCT1
FFFF	11 16 A9		JSP	LOUT2T
F601	30		PTS	
F602	0F 10 13	SUSPEND	LIX	#NEG1
F605	11 17 01		JSP	OUTSTF
F609	0F 10 10		LIX	#FAULT
F60F	11 17 01		JSP	OUTSTF
F60F	01	LF	NOP	
F60F	20 11		BPA	LF
		**	INTPT	-- 'INTERUPT ROUTINE'
F611	86 80		INTPT	LIA P
F613	15 11 00		PIT A	PIACFA
F616	26 11		PNE	STAPT2
F618	15 11 00		PIT A	PIACFE
F61F	26 03		PNE	HAITPT
F61F	11 14 17		JSP	FLPT

F620	2D	00	2F	HAITPT	TST	HTPT
F622	27	12			PEQ	INHOT
F625	26	07		OUTHOT	LDA A	OUT11
F627	16	03			LDA F	OUT1
F629	07	02			ADD F	#302
F62F	40	00			ADC A	#300
F62F	00				CLC	
F62F	46				POP A	
F62F	56				POP F	
F630	FD	F6	43		JSP	CVPTD
F633	0F				CLI	
F634	3F				FTI	
F635	7F	E4	9C	STARTP	JMP	START
F638	26	03		INHOT	LDA A	IN11
F63A	16	04			LDA F	IN1
F63C	00				CLC	
F63D	46				POP A	
F63E	56				POP F	
F63F	FD	F6	43		JSP	CVPTI
F642	3F				FTI	

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CVPTI -- CONVERSION OF BINARY TO  
DECIMAL

F642	02	16	6D	CVPTI	LIX	#K10K
F646	2F	00	23	CVDFC1	CLF	SAVEA
F649	10	01		CVDFC2	SUB F	10X
F64F	A2	00			SFC A	00X
F641	25	05			PCS	CVDFCE
F64F	7C	00	33		INC	SAVEA
F652	20	FF			FPA	CVDFC2
F654	11	01		CVDFCE	ALI F	10X
F656	A2	00			ADC A	00X
F658	26				PSH A	
F659	1F	24			STX	SAVEX1
F65F	26	32			LDA A	SAVEA
F65D	4F	20			ADD A	#330

MAKE ASCII CHAR

F65F	FD	F7	A9		JSP	OUTCH
F662	32				FUL A	RESTORE A
F663	1F	24			LIX	SAVEX1
F665	04				INX	
F666	04				INX	
F667	3C	F6	77		CFX	#K10K+10
F66A	26	1A			RNE	CVDFC1
F66C	20				PTS	

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CONSTANTS FOR CONVERSION

F66D	27	10		K10K	FDP	10000
F66F	02	F4			FDP	1000
F671	00	64			FDP	100
F673	00	0A			FDP	10
F675	00	01			FDP	1
F677	CF	E0	09	LCLCT1	LIX	#INDEX
F67A	16	02			LDA F	CNT2
F67C	08			LOOP	INX	
F67D	08				INX	
F67F	5A				DEC F	
F67F	26	FF			RNE	LOOP

F684	F6 01	LIIN1CT	LIA P	1,X
F686	FC		INC P	
F687	F7 01		STA P	1,X
F689	E6 00		LIA P	0,X
F691	C9 00		ADC P	#300
F68F	F7 00		STA P	0,X
F69F	39		PTS	
		**	LIIN2CT	-- 'LOCAL IN2COUNT'
		*		-- INCFEMENTS LOCAL IN2COUNT
F690	F6 02	LIIN2CT	LIA P	3,X
F692	FC		INC P	
F693	F7 02		STA P	3,X
F695	F6 02		LIA P	2,X
F697	C9 00		ADC P	#300
F699	F7 02		STA P	2,X
F69F	39		PTS	
		**	LOUT1T	-- 'LOCAL OUT1COUNT'
		*		-- INCFEMENTS LOCAL OUT1COUNT
F69C	F6 05	LOUT1T	LIA P	5,X
F69F	FC		INC P	
F69F	F7 05		STA P	5,X
F6A1	E6 04		LIA P	4,X
F6A2	C9 00		ADC P	#300
F6A5	F7 04		STA P	4,X
F6A7	39		PTS	
		**	LOUT2T	-- 'LOCAL OUT2COUNT'
		*		-- INCFEMENTS LOCAL OUT2COUNT
F6A4	F6 07	LOUT2T	LIA P	7,X
F6A4	FC		INC P	
F6A7	F7 07		STA P	7,X
F6A7	F6 06		LIA P	6,X
F6AF	C9 00		ADC P	#300
F6F1	E7 06		STA P	6,X
F6F3	39		PTS	
F6F4	DF 31	OFIGIN	STX	INDEX2
F6F6	06 02		LIA A	CNT2
F6F8	31 04		CMF A	#304
F6FA	27 23		PER	ISTTP
F6FC	31 03		CMF A	#303
F6FE	27 06		PER	STTP
F6C0	31 02		CMF A	#302
F6C2	27 3D		PER	TITTP
F6C4	20 32		PRA	FITTP
F6C6	06 30	STTP	LIA P	#380
F6C8	F5 F7 CA		HIT P	PIAOPB
F6CP	27 09		PER	FSFG2
F6CT	FD F7 21		JSP	SEARCH
F6D0	86 06		LIA A	#306
F6D2	FD F7 7F		JSP	PFL0AD
F6D5	39		PTS	
F6D6	FD F7 21	FSFG2	JSP	SEARCH
F6D9	86 02		LIA A	#302
F6DF	FD F7 7F		JSP	PFL0AD

F6DF	29		PTS	
F6EF	06 80	ISTTF	LIA P	#S80
F6F1	F5 F1 00		PIT P	FIADTF
F6F4	27 00		REC	FSPG1
F6F6	PD F7 21		JSP	SEAFCH
F6F9	86 05		LIA P	#305
F6FF	PD 17 71		JSP	PFLOAD
I6FF	29		PTS	
E6FF	PD F7 21	FSPG1	JSP	SEAFCH
F6F2	86 01		LIA P	#301
F6F4	PD F7 7F		JSP	PFLOAD
I6F7	29		PTS	
E6F8	PD F7 21	FITTF	JSP	SEAFCH
F6FF	86 04		LIA P	#304
E6F1	PD F7 7F		JSP	PFLOAD
F700	29		PTS	
F701	PD F7 21	TITTF	JSP	SEAFCH
F704	86 02		LIA P	#303
F706	PD F7 7F		JSP	PFLOAD
F709	29		PTS	
F70A	CF 00 02	CLFFT	LIX	#CLPIND
F70D	CF 00	CLFFT1	CLP	0,X
F70F	08		INX	
F710	8C 00 21		CFX	#CLFFI1+1
F712	26 F8		PNE	CLFFT1
		**	PUFCLF	-- 'PUFFER CLEAR'
		*		-- CLEARS THE BUFFERS
F715	CF 00 40	PUFCLF	LIX	#PUFIPT
F718	CF 00	PUFCLF1	CLP	0,X
F71A	08		INX	
F71D	8C 00 65		CFX	#PUFEND+1
F71F	26 F8		PNE	PUFCLP1
F720	29		PTS	
		**	SEAFCH	-- 'SEARCH'
		*		-- SEARCHES EMPTY BUFFER
		*		FOR LOADING IT
E721	7D 00 44	SEAFCH	TST	PUFFPT
F724	26 41		PNE	SEFCH2
F726	7D 00 42		TST	PUF4PT
F729	26 32		PNE	LD5PUF
F72B	7D 00 42		TST	PUF3PT
F72E	26 25		PNE	LI4PUF
F730	7D 00 41		TST	PUF2PT
F733	26 17		PNE	LD3PUF
F735	7D 00 40		TST	PUFIPT
F738	26 09		PNE	LD2PUF
		**	LD1PUF	-- 'LOAD THE FIRST BUFFER'
E73A	CF 00 47	LD1PUF	LIX	#1STPUF
F73D	DF 45		STX	PUFIND
F73F	7C 00 40		INC	PUFIPT
F742	29		PTS	
		**	LD2PUF	-- 'LOAD THE SECOND BUFFER'
E743	CF 00 4D	LD2PUF	LIX	#SNDEUF
F746	DF 45		STX	PUFIND
F748	7C 00 41		INC	PUF2PT

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F74C CE 00 52 L12PUF LIX #TH2PUF
F74F DF 4F STX PUFIND
F751 7C 00 42 INC PUF3PT
F754 39 PTS
** L142PUF -- "LOAD THE FOURTH BUFFER"
F755 CE 00 59 L142PUF LIX #FPTPUF
F758 DF 4F STX PUFIND
F75A 7C 00 42 INC PUF4PT
F75D 39 PTS
** L152PUF -- "LOAD THE FIFTH BUFFER"
F75E CE 00 5F L152PUF LIX #FFHPUF
F761 DF 4F STX PUFIND
F763 7C 00 44 INC PUF5PT
F766 39 PTS
F767 7D 00 40 SFFCH2 TST PUF1PT
F76A 27 CF PFG L11PUF
F76C 7D 00 41 TST PUF2PT
F76F 27 D2 PFG L12PUF
F771 7D 00 42 TST PUF3PT
F774 27 16 PFG L13PUF
F776 71 00 42 TST PUF4PT
F779 27 11 PFG L14PUF
F77B 7B 17 00 JMP PFFALT
** PFLCAL -- "BUFFER LOAD"
* -- LOAIS THE BUFFER FOR DISPLAY
F77E A7 00 PFLCAL STA A 0,X
F780 1F 31 LIX INDEX2
F782 A6 02 LIA A 2,X
F784 B6 03 LIA P 3,X
F786 DE 4F LIX PUFIND
F788 A7 01 STA A 1,X
F78A F7 02 STA P 2,X
F78C 1F 31 LIX INDEX2
F78E A6 04 LIA A 4,X
F790 B6 05 LIA P 5,X
F792 DE 4F LIX PUFIND
F794 A7 03 STA A 3,X
F796 F7 04 STA P 4,X
F798 39 PTS
F799 CF F2 48 PFFALT LIX #PUFFLT
F79C PI F7 CC JSP OUTSTP
F79F 7F F4 F7 JMP FLBT
** OUT4HS -- OUTPUT FOUR HEX DIGITS AND
* ENTPTY: -X> - ADDRESS OF BYTES
* EXIT: X INCREMENTED PAST BYTES
* USES: A,X
F7A2 81 11 OUT4HS PSP THE
** OUT2HS -- OUTPUT TWO HEX DIGITS AND
* ENTPTY,EXIT,USES -- SEE
F7A4 81 0F OUT2HS PSP THE
** OUTSF -- OUTPUT SPACE CODE
* ENTPTY: NONE; EXIT: <A> =
F7A6 86 20 OUTSF LIA A *
* OUTCH -- OUTPUT CHARACTER TO CONSOLE
* ENTPTY -- <A> = ASCII VALUE OF CHARACTER

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F7A8 27      OUTCH FSH F
F7A9 06 02    LDA F  #2
F7AB 55 FF 01 OUTT1  LIT F  ASCII
F7AD 27 FF    REC      OUTT1
F7AF 17 FF 0F  STA F  ASCII
F7B0 22      FUL F
F7B1 20      OUTT2  FTS
*
*      THP -- TYPE HEX BYTES
*      ENTRY : -X> - ADDRESS OF BYTE TO OUTPUT
*      EXIT  : -X> - OLIVALE+1
*      USES  : / 20
F7B5 86 00    TH1     LIA F  0,X
F7B7 08      INX
*
*      THP0 -- TYPE -A> IN HEX
*      ENTRY : -A> - VALUE
*      EXIT  : VALUE TYPE1
F7B8 26      THP0    FSH F
F7B9 22      LSF F
F7BA 22      LSF F
F7BB 22      LSF F
F7BC 22      LSF F
F7BD 22      LSF F
F7BE 81 02    PSH THP1
F7BF 22      FUL F
F7C0 82 0F    PSH F  #3F
F7C2 81 0A    THP1    CMP F  #10
F7C4 25 02    POC      THP2
F7C6 81 07    AII A  #7
F7C8 81 30    THP2    AII A  #30
F7CA 20 0C    OUTCHP  PFA      OUTCH
**      OUTSTF -- OUTPUT CHARACTER STRING TO C
*      ENTRY -- -X> - ADDRESS OF STRING
*      EXIT  -- -X> - INCREMENTED FAST END
*              END OF STRING MAPPER
*              A,X,C
F7CC 86 00    OUTSTF  LIA F  0,X
F7CE 08      INX
F7CF 81 F2    OUTST2  PSH      OUTCHP
F7D1 2A F2    PFL      OUTSTF
F7D3 22      OUTST3  FTS
F7D4      ENI

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STATEMENTS -826

FFFF BYTES -11158

NO ERRORS DETECTED

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